## Significant Rare Earths system further confirmed at Neo prospect, Paddy's Well Project.

## Highlights

- Multiple holes with significant mineralised REE intercepts ( $\sim 80 \mathrm{~m}$ ) from surface; potentially some of widest reported in Australia", alluding to large scale \& "open pit" potential.
- Mineralisation remains open at depth and along strike.
- Encouraging high ratio of in-demand 'magnet' ${ }^{2}$ REEs to TREO ('Magnet REO') (peak: 30\%)
- Metallurgical testing underway to characterise the REE species present - positive 'size by assay' results have been received and are under review.

Voltaic Strategic Resources Limited (ASX:VSR) has confirmed the scale potential of the Neo Prospect at its Paddy Well Project in Western Australia's Gascoyne region after encountering several further extremely wide REE mineralised intercepts from surface. Assays from another 12 RB drillholes from the Phase-1B campaign show intercepts of almost 80 m from surface across multiple holes, with mineralisation remaining open at depth and along strike.

Neo forms part of an expanding regional $6 \times 2 \mathrm{~km}$ anomalous area with multiple $>1,000 \mathrm{ppm}$ TREO zones identified at surface and only a fraction of the area tested to date (Fig. 3). Encouragingly, drilling returned individual metre values up to $1 \%$ TREO, and high tenor 'magnet REE' percentages up to $30 \%$.

Work commenced earlier this year to test the upper clay zone and determine basement depth within an area where historical uranium-focused drilling identified REEs in both the upper oxide (clay) horizon, and primary REE mineralisation in deeper basement ${ }^{3}$.

## Voltaic Chief Executive Officer Michael Walshe commented:

"We now have unequivocal evidence for the presence of a large alumina-rich, kaolinitic REE clay system at Neo, which has the potential for hosting a near-surface "open-pittable" REE clay deposit of substantial scale ${ }^{1}$."
"Metallurgical testing on the clays is now underway to determine their preliminary economic viability and ion-absorption (IAD) potential. The ‘size by assay’ analysis work has been completed and the preliminary results are encouraging for a significant upgrade in REE grades and the removal of waste, by undertaking simple upstream mineral processing techniques ${ }^{4}$.

[^0]"The leach testwork is due to commence next week once this data has been reviewed and a decision made on the optimal size fraction for leaching. Encouragingly, halloysite has already been identified ${ }^{5}$ from scanning electron microscope (SEM) analysis (Fig. 10), which is a kaolinitic clay mineral commonly found in true IAD clays."
"Simultaneously, in the field our focus is now on primary carbonatite targets. We will soon undertake several field surveys including: airborne magnetics / radiometrics, photogrammetry, and soil sampling. These programs will increase our pool of priority targets and ensure several months of highly active and material news flow over the remainder of 2023."


Figure 1. Location of the Neo prospect area, Paddys Well project.

[^1]Significant assay results from 14-hole Phase 1B campaign ${ }^{6}$ :

| DRILL HOLE |  | INTERSECTION |
| :---: | :---: | :---: |
| NEORB002 | incl: <br> and: <br> with peak of: | 78m @ 1,001ppm TREO (from surface NEORB002) <br> 52m @ 1,270ppm TREO (from 21m) <br> 12m @ 3,402ppm TREO (from 50m) <br> 1m @ 10,072ppm TREO (1.01\% TREO) (from 56m) |
| NEORB003 | incl: <br> incl: <br> with peak of: | ```78m @ 661ppm TREO (from surface NEORB003) 3m @ 1,187ppm TREO (from 53m) 1m @ 1,410ppm TREO (from 77m EOH) 1m@ 2,046ppm TREO (from 54m)``` |
| NEORB008 | incl: with peak of: | ```75m @ 521ppm TREO (from surface NEORB008) 3m @ 1,009ppm TREO (from 42m) 1m@ 1,263ppm TREO (from 13m)``` |
| NEORB006 | incl: <br> with peak of: | ```65m @ 546ppm TREO (from surface NEORB006) 18m @ 1,018ppm TREO (from 34m) 1m @ 1,899ppm TREO (from 46m)``` |
| NEORB013 | incl: | 63m @ 582ppm TREO (from surface NEORB013) 4m @ 1,143ppm TREO (from 49m) |
| NEORB004 | incl: with peak of: | 60m @ 491ppm TREO (from surface NEORB004) <br> 12m @ 636 ppm TREO (from 67m) <br> 1m @ 2,045ppm TREO (from 68m) |
| NEORB014 | incl: <br> with peak of: | 59m @ 878ppm TREO (from surface NEORB014) <br> 5m @ 1,758ppm TREO (from 18m) <br> 1m @ 2,827ppm TREO (from 22m) |
| NEORB005 | incl: <br> with peak of: | ```33m @ 756ppm TREO (from surface NEORB005) 12m @ 1,004ppm TREO (from 21m) 1m @ 3,766ppm TREO (from 32m)``` |

[^2]No further clay-focused drilling is planned until the leaching results are known, which the Company believes is the most prudent use of capital going forward, and concurrently, exploration continues focusing on the Company's several primary carbonatite REE \& niobium targets within Paddys Well (see Fig. 2).

## CONCURRENT TARGETS

AT PADDYS WELL


Cease focus on clay system at Neo \& divert attention to primary hardrock / carbonatite REE \& Niobium targets
"Unsuccessful"


Figure 2. The strategy ahead at Paddy's Well


Figure 3. TREO contours at the Neo prospect within regional $6 \times 2 \mathrm{~km}$ anomalous area with multiple $>1,000 \mathrm{ppm}$ TREO zones identified at surface and only a fraction of the area tested to date.

# Release authorised by the Board of Voltaic Strategic Resources Ltd. 

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Upcoming News Flow
June/July 2023: Paddys Well geophysical data (radiometric / magnetic / photogrammetry) acquisition update
June/July 2023: Further drill sample assays from Link prospects
June/July 2023: Update on Metallurgical testing of REE-enriched clays from Neo

PLanned and completed activities at Paddys Well: Q2-Q3 2023


## Competent Person Statement

The information in this announcement related to Exploration Results is based on and fairly represents information compiled by Mr Claudio Sheriff-Zegers. Mr Sheriff-Zegers is employed as an Exploration Manager for Voltaic Strategic Resources Ltd and is a member of the Australasian Institute of Mining and Metallurgy. He has sufficient experience of relevance to the styles of mineralisation and types of deposits under consideration and to the activities undertaken to qualify as a Competent Person as defined in the 2012 Edition of the Joint Ore Reserves Committee (JORC) Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. He consents to the inclusion in this announcement of the matters based on information in the form and context in which they appear.

The information in this document that relates to metallurgical test work and flowsheet development is based on, and fairly represents, information and supporting documentation reviewed by Mr Michael Walshe. Mr Walshe is engaged as Chief Executive Officer for Voltaic Strategic Resources Ltd. He holds a Bachelor of Chemical and Process Engineering (Hons.) and a Master of Business Administration (Finance). He is a chartered engineer with both Engineers Australia \& the Institution of Chemical Engineers (IChemE), and is a member of the Australasian Institute of Mining \& Metallurgy (AusIMM). He has over 15 years of experience in process engineering and metallurgy across a wide range of commodities including rare earths, and has approved and consented to the inclusion in this document of the matters based on his information in the form and context in which it appears.

## Forward-LOOKING Statements

This announcement may contain forward-looking statements involving several risks and uncertainties. These forward-looking statements are expressed in good faith and believed to have a reasonable basis. These statements reflect current expectations, intentions or strategies regarding the future and assumptions based on currently available information. Should one or more of the risks or uncertainties materialise, or underlying assumptions prove incorrect, actual results may vary from the expectations, intentions and strategies described in this announcement. No obligation is assumed to update statements if these beliefs, opinions, and estimates should change or to reflect other future development. Furthermore, this announcement contains forward-looking statements which may be identified by words such as "potential", "believes", "estimates", "expects', "intends", "may", "will", "would", "could", or "should" and other similar words that involve risks and uncertainties. These statements are based on a number of assumptions regarding future events and actions that, as at the date of this announcement, are expected to take place. Such forward-looking statements are not guarantees of future performance and involve known and unknown risks, uncertainties, assumptions and other important factors, many of which are beyond the control of the Company, the Directors and management of the Company. These and other factors could cause actual results to differ materially from those expressed in any forwardlooking statements. The Company cannot and does not give assurances that the results, performance, or achievements expressed or implied in the forwardlooking statements contained in this announcement will actually occur and investors are cautioned not to place undue reliance on these forward-looking statements.

## About Voltaic Strategic Resources

Voltaic Strategic Resources Limited explore for the next generation of mines that will produce the metals required for a cleaner, more sustainable future where transport is fully electrified, and renewable energy represents a greater share of the global energy mix.

The company has a strategically located critical metals portfolio led by lithium, rare earths, base metals, and gold across two of the world's most established mining jurisdictions: Western Australia \& Nevada, USA.

Voltaic is led by an accomplished corporate and technical team with extensive experience in REEs, lithium and other critical minerals, and a strong skillset in both geology and processing / metallurgy.


## Appendix 1 Drill data

Table 1. Neo blade/reverse circulation (RB) drilling - lab assay results, significant intersections

| Hole | From (m) | To <br> (m) | Interval (m) | TREO* (ppm) | TREO intercept (ppm) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NEORC001 | 0 | 40 | 40 | 583 | 40m @ 583ppm TREO (from surface NEORC001) |
| NEORB002 | 0 | 78 | 78 | 1,001 | 78m@ 1,001ppm TREO (from surface NEORB002) |
|  | 0 | 14 | 14 | 629 | 14m@ 629ppm TREO (from surface) |
|  | 21 | 72 | 52 | 1,270 | 52 m @ 1,270ppm TREO (from 21m) |
|  | 50 | 61 | 12 | 3,402 | 12m @ 3,402ppm TREO (from 50m) |
|  | 55 | 56 | 1 | 10,072 | $1 \mathrm{~m} @ 10,072 \mathrm{ppm}$ TREO (1.01\% TREO) (from 55m) |
| NEORB003 | 0 | 78 | 78 | 661 | 78m @ 661ppm TREO (from surface NEORB003) |
|  | 4 | 13 | 9 | 985 | 9m@ 985ppm TREO (from 4m) |
|  | 17 | 21 | 4 | 760 | $4 \mathrm{~m} @ 760 \mathrm{ppm}$ TREO (from 17m) |
|  | 28 | 33 | 5 | 1,151 | 5m@ 1,151ppm TREO (from 28m) |
|  | 31 | 32 | 1 | 1,977 | 1m@ 1,977ppm TREO (from 31m) |
|  | 36 | 49 | 13 | 601 | 13m @ 601ppm TREO (from 36m) |
|  | 53 | 56 | 3 | 1,187 | 3m@ 1,187ppm TREO (from 53m) |
|  | 54 | 55 | 1 | 2,046 | 1m@ 2,046ppm TREO (from 54m) |
|  | 58 | 79 | 21 | 679 | 21m @ 679ppm TREO (from 58m) |
|  | 64 | 67 | 3 | 851 | 3m@ 851ppm TREO (from 64m) |
|  | 64 | 65 | 1 | 1,037 | 1m@ 1,037ppm TREO (from 64m) |
|  | 74 | 79 | 5 | 816 | 5m@ 816ppm TREO (from 74m) |
|  | 77 | 78 | 1 | 1,410 | $1 \mathrm{~m} @ 1,410 \mathrm{ppm}$ TREO (from 77m EOH) |
| NEORB004 | 0 | 60 | 60 | 491 | 60m @ 491ppm TREO (from surface NEORB004) |
|  | 28 | 34 | 6 | 800 | 6 m @ 800ppm TREO (from 28m) |
|  | 47 | 55 | 8 | 664 | 8m @ 664ppm TREO (from 47m) |
|  | 67 | 79 | 12 | 636 | 12m @ 636ppm TREO (from 67m) |
|  | 68 | 69 | 1 | 2,045 | 1m@ 2,045ppm TREO (from 68m) |
|  | 74 | 78 | 4 | 753 | 4m@ 753ppm TREO (from 74m) |
|  | 77 | 78 | 1 | 1,133 | 1m@ 1,133ppm TREO (from 77m) |
| NEORB005 | 0 | 33 | 33 | 756 | 33m @ 756ppm TREO (from surface NEORB005) |
|  | 5 | 15 | 10 | 861 | 10m @ 861ppm TREO (from 5m) |
|  | 13 | 14 | 1 | 1,063 | 1 m @ 1,063ppm TREO (from 13m) |
|  | 21 | 33 | 12 | 1,004 | 12m @ 1,004ppm TREO (from 21m) |
|  | 31 | 33 | 2 | 2,994 | 2m@ 2,994ppm TREO (from 31m) |
|  | 32 | 33 | 1 | 3,766 | 1m@3,766ppm TREO (from 32m) |
| NEORB006 | 0 | 65 | 65 | 546 | 65m @ 546ppm TREO (from surface NEORB006) |
|  | 34 | 57 | 23 | 914 | 23m@ 914ppm TREO (from 34m) |
|  | 34 | 52 | 18 | 1,018 | 18m @ 1,018ppm TREO (from 34m) |
|  | 43 | 51 | 8 | 1,216 | 8m @ 1,216ppm TREO (from 43m) |
|  | 46 | 47 | 1 | 1,899 | 1m@ 1,899ppm TREO (from 46m) |
| NEORB007 | 0 | 12 | 12 | 493 | 12m @ 493ppm TREO (from surface NEORB007) |
|  | 5 | 8 | 3 | 844 | 3m @ 844ppm TREO (from 5m) |
|  | 5 | 6 | 1 | 1,413 | 1m@ 1,413ppm TREO (from 5m) |
|  | 17 | 64 | 47 | 431 | 47m @ 431ppm TREO (from 17m) |
|  | 41 | 42 | 1 | 1,049 | 1m@ 1,049ppm TREO (from 41m) |
|  | 49 | 63 | 14 | 639 | 14m @ 639ppm TREO (from 49m) |
|  | 57 | 58 | 1 | 1,002 | 1m@ 1,002ppm TREO (from 57m) |


| Hole | From (m) | $\begin{aligned} & \text { To } \\ & \text { (m) } \\ & \hline \end{aligned}$ | Interval <br> (m) | TREO* (ppm) | TREO intercept (ppm) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NEORB008 | 0 | 75 | 75 | 521 | 75m @ 521ppm TREO (from surface NEORB008) |
|  | 13 | 29 | 16 | 747 | 16m @ 747ppm TREO (from 13m) |
|  | 13 | 21 | 8 | 948 | 8m @ 948ppm TREO (from 13m) |
|  | 13 | 14 | 1 | 1,263 | 1m@ 1,263ppm TREO (from 13m) |
|  | 16 | 17 | 1 | 1,104 | 1m@ 1,104ppm TREO (from 16m) |
|  | 38 | 54 | 16 | 697 | 16m @ 697ppm TREO (from 38m) |
|  | 42 | 45 | 3 | 1,009 | 3m @ 1,009ppm TREO (from 42m) |
|  | 43 | 44 | 1 | 1,157 | 1m@ 1,157ppm TREO (from 43m) |
| NEORB009 | 0 | 4 | 4 | 358 | 4m@ 358ppm TREO (from surface NEORB009) |
|  | 9 | 11 | 2 | 322 | 2m@ 322ppm TREO (from 9m) |
| NEORB010 | 0 | 10 | 10 | 356 | 10m @ 356ppm TREO (from surface NEORB010) |
|  | 6 | 7 | 1 | 1,240 | 1m@ 1,240ppm TREO (from 6m) |
| NEORB011 | 0 | 7 | 7 | 574 | 7m@ 574ppm TREO (from surface NEORB011) |
|  | 7 | 8 | 1 | 791 | 1m@ 791ppm TREO (from 7m) |
| NEORB012 | 0 | 28 | 28 | 447 | 28m @ 447ppm TREO (from surface NEORB012) |
|  | 5 | 8 | 3 | 703 | 3m@ 703ppm TREO (from 5m) |
|  | 25 | 28 | 3 | 708 | 3 m @ 708ppm TREO (from 25m) |
| NEORB013 | 0 | 63 | 63 | 582 | 63m @ 582ppm TREO (from surface NEORB013) |
|  | 41 | 63 | 22 | 741 | 22m@ 741ppm TREO (from 41m) |
|  | 49 | 53 | 4 | 1,143 | 4m@ 1,143ppm TREO (from 49m) |
| NEORB014 | 0 | 59 | 59 | 878 | 59m @ 878ppm TREO (from surface NEORB014) |
|  | 11 | 13 | 2 | 1,285 | 2m@ 1,285ppm TREO (from 11m) |
|  | 12 | 13 | 1 | 1,502 | 1m@ 1,502ppm TREO (from 12m) |
|  | 18 | 23 | 5 | 1,758 | 5m@ 1,758ppm TREO (from 18m) |
|  | 22 | 23 | 1 | 2,827 | 1m@ 2,827ppm TREO (from 22m) |
|  | 24 | 32 | 8 | 1,195 | 8m @ 1,195ppm TREO (from 24m) |
|  | 31 | 32 | 1 | 1,944 | 1m@ 1,944ppm TREO (from 31m) |
|  | 53 | 58 | 5 | 1,137 | 5m@ 1,137ppm TREO (from 53m) |
|  | 56 | 57 | 1 | 2,122 | $1 \mathrm{~m} @ 2,122 \mathrm{ppm}$ TREO (from 56m) |

[^3]

Figure 4. Neo section 374500E - cross section significant intercepts


Figure 5. Neo 374460E cross section significant intercepts


Figure 6. Neo $374590 E$ cross section significant intercepts


Figure 7. Neo 374415E cross section significant intercepts

| $7.257,600 \mathrm{mN}$ | $\begin{aligned} & \text { 唇 } \\ & \text { 辟 } \end{aligned}$ |  |  | $\begin{aligned} & \text { 唇 } \\ & \text { 窘 } \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Neo | $\qquad$ | ${ }^{\text {－}}$（EORB009 |  | VOLTAIC <br> －Neo drill collars <br> REE Prospect |
|  |  | NEORB014 | NEORC001 NEORB002 | ${ }^{\text {NEORB008 }}$ | NEORB011 －${ }^{\text {NEORB010 }}$ |  |
| 7.257 .500 mN | ＋ | ${ }^{\text {－}}$－${ }^{\text {arbio13 }}$ | NEORB003 | ${ }^{\text {neorboop }}{ }^{\text {a }}$ |  | $7.257,500 \mathrm{mN}$ |
|  |  |  | ${ }^{\bullet}$ NEORB012 |  |  |  |
|  |  | $\bar{s}$ | $\begin{aligned} & \text { 唇 } \\ & \text { 枈 } \end{aligned}$ | $\begin{aligned} & \text { 唇 } \\ & \text { 長 } \end{aligned}$ | $\begin{aligned} & \text { 唇 } \\ & \stackrel{\rightharpoonup}{2} \end{aligned}$ |  |

Figure 8．Map plan showing drill collars at the Neo prospect．


Figure 9．Aerial photo of the Neo prospect area，Paddys Well project．


Figure 10. Halloysite nanotubes \& associated kaolin ${ }^{7}$ identified from SEM analysis of REE-enriched clay samples from historical drillhole GAD0004 ${ }^{8}$. Halloysite is a common kaolinitic clay mineral ( $\mathrm{Al}_{2} \mathrm{O}_{3} \cdot 2 \mathrm{SiO}_{2} \cdot 2 \mathrm{H}_{2} \mathrm{O}$ ) found in true REE ionic adsorption deposits (IADs) ${ }^{9}$

[^4]
## Appendix 2 Supplementary Data

Table 2. Neo phase 1B drilling summary

| Hole ID | Easting GDA_94 | Northing GDA_94 | RL | Mag Azimuth | Dip | Depth (m) | Prospect | Drill Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NEORC001 | 374497 | 7257528 | 341 | 010 | -60 | 40 | Neo | RC |
| NEORB002 | 374497 | 7257528 | 341 | 0 | -90 | 78 | Neo | RB |
| NEORB003 | 374496 | 7257494 | 341 | 0 | -90 | 78 | Neo | RB |
| NEORB004 | 374505 | 7257572 | 341 | 0 | -90 | 78 | Neo | RB |
| NEORB005 | 374412 | 7257538 | 341 | 0 | -90 | 35 | Neo | RB |
| NEORB006 | 374420 | 7257578 | 341 | 0 | -90 | 65 | Neo | RB |
| NEORB007 | 374580 | 7257507 | 341 | 0 | -90 | 63 | Neo | RB |
| NEORB008 | 374589 | 7257547 | 341 | 0 | -90 | 75 | Neo | RB |
| NEORB009 | 374591 | 7257594 | 341 | 0 | -90 | 15 | Neo | RB |
| NEORB010 | 374682 | 7257537 | 341 | 0 | -90 | 11 | Neo | RB |
| NEORB011 | 374681 | 7257566 | 341 | 0 | -90 | 17 | Neo | RB |
| NEORB012 | 374489 | 7257442 | 341 | 0 | -90 | 32 | Neo | RB |
| NEORB013 | 374457 | 7257508 | 341 | 0 | -90 | 63 | Neo | RB |
| NEORB014 | 374458 | 7257551 | 341 | 0 | -90 | 60 | Neo | RB |

Table 3. Rare Earth Element Assay Results (as Oxides) from Phase 1B Campaign

| Hole ID | From (m) | $\begin{aligned} & \hline \text { To } \\ & \text { (m) } \end{aligned}$ | $\begin{aligned} & \text { TREO } \\ & \text { (ppm) } \end{aligned}$ | MREO TREO $\qquad$ | $\mathrm{Nd}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{PrgO}_{11} \mathrm{O}_{1} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Tb}_{4} \mathrm{O}_{7} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \mathrm{Dy}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{array} \end{aligned}$ | $\begin{aligned} & \hline \mathrm{La}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{gathered} \mathrm{CeO}_{2} \\ (\mathrm{ppm}) \end{gathered}$ | $\mathrm{Sm}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{Eu}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Cd}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Ho}_{2} \mathrm{O}_{3} \\ & \text { (ppm) } \end{aligned}$ | $\begin{aligned} & \mathrm{Er}_{\mathrm{r}, \mathrm{O}_{3}} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \hline \mathrm{Tm}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \hline \mathrm{Yb}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{L}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{gathered} \mathrm{Y}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NEORB002 | 0 | 1 | 422 | 21.6\% | 67.3 | 21.0 | 0.6 | 2.3 | 94.6 | 196.8 | 11.1 | 1.3 | 5.5 | 0.4 | 0.9 | 0.1 | 0.6 | 0.1 | 10.2 |
|  | 1 | 2 | 633 | 21.6\% | 102.3 | 30.7 | 0.8 | 3.2 | 147.8 | 291.7 | 16.2 | 1.6 | 7.8 | 0.5 | 1.1 | 0.1 | 0.8 | 0.1 | 14.3 |
|  | 2 | 3 | 733 | 21.5\% | 116.6 | 36.6 | 1.0 | 3.8 | 167.7 | 343.2 | 18.4 | 1.7 | 9.6 | 0.5 | 1.2 | 0.1 | 0.7 | 0.1 | 15.4 |
|  | 3 | 4 | 871 | 22.0\% | 142.3 | 43.5 | 1.2 | 4.4 | 207.6 | 395.9 | 23.0 | 2.0 | 11.8 | 0.6 | 1.3 | 0.1 | 0.8 | 0.1 | 17.4 |
|  | 4 | 5 | 644 | 22.2\% | 105.7 | 32.7 | 1.0 | 3.9 | 147.8 | 292.8 | 17.6 | 1.4 | 8.9 | 0.5 | 1.2 | 0.1 | 0.8 | 0.1 | 15.0 |
|  | 5 | 6 | 655 | 21.8\% | 106.0 | 33.0 | 0.9 | 3.1 | 152.5 | 303.4 | 16.7 | 1.2 | 8.3 | 0.5 | 0.9 | 0.1 | 0.5 | 0.1 | 13.0 |
|  | 6 | 7 | 597 | 22.7\% | 101.7 | 30.7 | 0.7 | 2.2 | 137.2 | 278.8 | 14.6 | 1.2 | 6.9 | 0.3 | 0.6 | 0.1 | 0.4 | 0.1 | 8.0 |
|  | 7 | 8 | 417 | 22.8\% | 71.4 | 21.3 | 0.5 | 1.8 | 92.2 | 194.4 | 10.8 | 1.0 | 5.5 | 0.2 | 0.6 | 0.1 | 0.4 | 0.0 | 7.0 |
|  | 8 | 9 | 279 | 21.7\% | 45.0 | 13.7 | 0.4 | 1.3 | 61.0 | 132.4 | 7.6 | 0.7 | 3.8 | 0.2 | 0.4 | 0.0 | 0.3 | 0.1 | 5.2 |
|  | 9 | 10 | 834 | 22.7\% | 142.3 | 41.7 | 1.0 | 4.3 | 190.0 | 381.8 | 21.2 | 1.6 | 10.5 | 0.6 | 1.4 | 0.2 | 1.1 | 0.2 | 17.4 |
|  | 10 | 11 | 1,169 | 23.0\% | 200.6 | 61.4 | 1.4 | 5.0 | 261.5 | 542.3 | 29.2 | 2.0 | 13.6 | 0.7 | 1.6 | 0.2 | 1.2 | 0.2 | 21.7 |
|  | 11 | 12 | 702 | 22.7\% | 119.0 | 37.0 | 0.8 | 2.9 | 157.2 | 329.1 | 17.4 | 1.4 | 8.4 | 0.4 | 0.8 | 0.1 | 0.6 | 0.1 | 11.2 |
|  | 12 | 13 | 339 | 22.2\% | 56.6 | 16.7 | 0.4 | 1.5 | 73.9 | 161.6 | 8.4 | 1.0 | 4.1 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 6.0 |
|  | 13 | 14 | 509 | 22.6\% | 85.7 | 26.2 | 0.6 | 2.4 | 115.9 | 234.3 | 13.2 | 1.4 | 6.5 | 0.4 | 0.8 | 0.1 | 0.6 | 0.1 | 9.3 |
|  | 14 | 15 | 227 | 22.2\% | 37.7 | 11.2 | 0.3 | 1.2 | 53.9 | 101.7 | 6.1 | 1.0 | 3.0 | 0.2 | 0.4 | 0.1 | 0.4 | 0.1 | 5.1 |
|  | 15 | 16 | 255 | 21.8\% | 41.4 | 12.7 | 0.4 | 1.3 | 57.5 | 119.5 | 6.4 | 1.1 | 3.3 | 0.2 | 0.5 | 0.1 | 0.4 | 0.0 | 4.9 |
|  | 16 | 20 | 283 | 22.2\% | 47.1 | 13.8 | 0.4 | 1.5 | 61.0 | 133.5 | 7.1 | 1.2 | 3.5 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 5.7 |
|  | 20 | 21 | 740 | 22.7\% | 126.0 | 38.1 | 0.8 | 3.0 | 164.2 | 347.9 | 18.6 | 1.6 | 8.5 | 0.4 | 0.9 | 0.1 | 0.8 | 0.1 | 12.0 |
|  | 21 | 22 | 316 | 23.2\% | 54.8 | 16.7 | 0.4 | 1.4 | 73.2 | 142.9 | 8.2 | 1.3 | 3.8 | 0.2 | 0.4 | 0.1 | 0.4 | 0.0 | 5.5 |
|  | 22 | 23 | 303 | 23.2\% | 52.4 | 16.1 | 0.4 | 1.5 | 67.1 | 139.4 | 7.8 | 1.3 | 3.6 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 5.5 |
|  | 23 | 24 | 201 | 23.2\% | 34.8 | 10.5 | 0.3 | 1.0 | 44.8 | 91.6 | 5.1 | 1.2 | 2.5 | 0.1 | 0.3 | 0.0 | 0.3 | 0.0 | 3.5 |
|  | 24 | 25 | 438 | 23.2\% | 75.5 | 23.0 | 0.6 | 2.4 | 92.4 | 202.6 | 12.1 | 1.7 | 5.9 | 0.4 | 1.0 | 0.1 | 0.8 | 0.1 | 9.1 |
|  | 25 | 26 | 692 | 23.2\% | 120.1 | 36.0 | 0.9 | 3.6 | 150.1 | 320.9 | 17.9 | 1.8 | 8.9 | 0.5 | 1.3 | 0.2 | 1.3 | 0.2 | 13.0 |
|  | 26 | 27 | 973 | 22.7\% | 166.8 | 49.5 | 1.0 | 3.6 | 226.4 | 449.8 | 23.9 | 2.1 | 11.5 | 0.5 | 1.1 | 0.1 | 0.9 | 0.1 | 14.1 |
|  | 27 | 28 | 441 | 22.7\% | 75.6 | 22.6 | 0.5 | 1.6 | 101.8 | 205.0 | 11.1 | 1.4 | 5.0 | 0.2 | 0.4 | 0.1 | 0.4 | 0.1 | 5.7 |
|  | 28 | 29 | 1,042 | 22.6\% | 177.3 | 53.9 | 1.0 | 3.7 | 241.6 | 483.7 | 25.5 | 2.2 | 11.4 | 0.5 | 1.3 | 0.2 | 1.2 | 0.2 | 14.2 |
|  | 29 | 30 | 566 | 23.4\% | 99.1 | 30.2 | 0.6 | 2.4 | 124.3 | 261.2 | 14.6 | 2.0 | 6.3 | 0.4 | 1.1 | 0.1 | 1.2 | 0.2 | 9.7 |
|  | 30 | 31 | 544 | 23.0\% | 93.7 | 28.0 | 0.6 | 2.7 | 120.8 | 249.5 | 13.8 | 1.9 | 6.8 | 0.4 | 1.0 | 0.1 | 1.0 | 0.2 | 11.3 |
|  | 31 | 32 | 396 | 23.1\% | 68.7 | 20.3 | 0.5 | 1.9 | 87.8 | 181.6 | 10.3 | 1.9 | 4.9 | 0.3 | 0.6 | 0.1 | 0.5 | 0.1 | 8.1 |
|  | 32 | 33 | 260 | 23.4\% | 45.5 | 13.8 | 0.3 | 1.3 | 56.3 | 118.3 | 7.3 | 1.7 | 3.3 | 0.2 | 0.5 | 0.0 | 0.4 | 0.1 | 5.0 |
|  | 33 | 34 | 526 | 22.7\% | 88.8 | 27.1 | 0.7 | 2.7 | 114.1 | 244.8 | 13.9 | 2.0 | 6.8 | 0.4 | 0.9 | 0.1 | 0.8 | 0.1 | 10.6 |
|  | 34 | 35 | 139 | 22.7\% | 23.2 | 6.7 | 0.5 | 1.2 | 26.3 | 64.7 | 4.3 | 0.6 | 2.7 | 0.2 | 0.6 | 0.1 | 0.5 | 0.1 | 4.8 |
|  | 35 | 36 | 895 | 23.1\% | 155.1 | 47.6 | 0.9 | 3.4 | 195.9 | 420.5 | 23.7 | 2.8 | 10.1 | 0.5 | 1.1 | 0.1 | 0.9 | 0.1 | 11.9 |
|  | 36 | 37 | 588 | 22.9\% | 101.0 | 30.2 | 0.7 | 2.6 | 126.7 | 277.6 | 15.8 | 1.8 | 7.6 | 0.4 | 0.7 | 0.1 | 0.6 | 0.1 | 9.1 |
|  | 37 | 38 | 490 | 22.6\% | 82.7 | 25.4 | 0.6 | 2.3 | 108.7 | 228.4 | 12.6 | 1.9 | 6.1 | 0.4 | 0.7 | 0.1 | 0.6 | 0.1 | 8.4 |
|  | 38 | 39 | 364 | 23.2\% | 63.5 | 19.3 | 0.4 | 1.4 | 79.6 | 171.0 | 9.2 | 1.9 | 3.9 | 0.2 | 0.4 | 0.0 | 0.3 | 0.0 | 4.8 |
|  | 39 | 40 | 291 | 22.8\% | 49.7 | 15.2 | 0.3 | 1.1 | 64.7 | 135.9 | 7.8 | 1.7 | 3.3 | 0.1 | 0.3 | 0.0 | 0.2 | 0.0 | 3.6 |
|  | 40 | 44 | 319 | 23.4\% | 56.3 | 16.4 | 0.4 | 1.4 | 69.3 | 147.6 | 8.6 | 1.8 | 3.7 | 0.2 | 0.4 | 0.0 | 0.3 | 0.1 | 4.9 |
|  | 44 | 45 | 505 | 23.2\% | 87.8 | 26.5 | 0.6 | 2.4 | 110.1 | 233.1 | 13.1 | 1.8 | 5.8 | 0.4 | 0.9 | 0.1 | 0.8 | 0.1 | 9.9 |
|  | 45 | 46 | 707 | 22.7\% | 119.0 | 37.6 | 0.8 | 3.5 | 152.5 | 332.6 | 16.9 | 2.5 | 7.7 | 0.5 | 1.3 | 0.2 | 1.3 | 0.2 | 14.6 |
|  | 46 | 47 | 848 | 22.4\% | 140.0 | 44.0 | 1.2 | 5.0 | 183.0 | 394.7 | 20.1 | 3.2 | 10.0 | 0.8 | 2.0 | 0.3 | 1.9 | 0.3 | 22.5 |
|  | 47 | 48 | 721 | 22.1\% | 116.6 | 38.4 | 0.9 | 3.7 | 156.0 | 342.0 | 16.8 | 2.7 | 7.8 | 0.6 | 1.4 | 0.2 | 1.3 | 0.2 | 15.9 |
|  | 48 | 49 | 916 | 22.9\% | 154.0 | 49.1 | 1.3 | 5.5 | 194.7 | 422.8 | 23.0 | 3.6 | 11.2 | 0.9 | 2.2 | 0.3 | 2.2 | 0.3 | 24.9 |
|  | 49 | 50 | 1,128 | 23.1\% | 192.5 | 59.6 | 1.5 | 6.6 | 236.9 | 523.6 | 28.4 | 4.7 | 13.8 | 0.9 | 2.4 | 0.3 | 2.1 | 0.3 | 29.3 |
|  | 50 | 51 | 1,630 | 23.9\% | 285.8 | 90.9 | 2.4 | 10.1 | 344.8 | 730.9 | 43.4 | 7.3 | 21.8 | 1.6 | 4.2 | 0.5 | 3.8 | 0.5 | 46.5 |
|  | 51 | 52 | 2,186 | 22.8\% | 367.4 | 116.3 | 2.9 | 12.3 | 424.6 | 1,050.7 | 56.4 | 9.5 | 27.0 | 1.9 | 4.6 | 0.6 | 3.9 | 0.6 | 55.7 |
|  | 52 | 53 | 2,408 | 28.0\% | 496.9 | 153.4 | 4.5 | 19.4 | 585.2 | 886.7 | 78.7 | 15.5 | 37.7 | 2.8 | 6.9 | 0.9 | 5.4 | 0.7 | 70.4 |
|  | 53 | 54 | 1,775 | 21.9\% | 286.9 | 90.7 | 2.1 | 8.9 | 337.8 | 885.5 | 43.9 | 7.6 | 20.1 | 1.4 | 3.3 | 0.4 | 2.7 | 0.4 | 40.5 |
|  | 54 | 55 | 9,625 | 25.9\% | 1,854.6 | 584.8 | 11.2 | 39.0 | 2,545.0 | 3,865.3 | 238.9 | 55.1 | 114.3 | 4.8 | 9.0 | 0.8 | 3.9 | 0.4 | 109.1 |
|  | 55 | 56 | 10,072 | 29.9\% | 2,204.5 | 685.0 | 23.5 | 97.0 | 1,630.2 | 4,205.0 | 365.3 | 92.1 | 199.4 | 14.0 | 31.6 | 3.9 | 23.1 | 2.9 | 289.5 |
|  | 56 | 57 | 4,662 | 30.1\% | 1,027.6 | 317.8 | 11.4 | 48.0 | 716.6 | 1,920.9 | 175.1 | 41.7 | 98.9 | 7.0 | 16.7 | 2.1 | 12.6 | 1.6 | 170.2 |
|  | 57 | 58 | 2,715 | 24.5\% | 487.6 | 151.0 | 4.9 | 21.0 | 322.5 | 1,417.3 | 80.9 | 17.8 | 42.4 | 3.2 | 7.3 | 1.0 | 6.5 | 0.9 | 81.4 |
|  | 58 | 59 | 1,885 | 23.1\% | 318.4 | 98.8 | 3.3 | 14.9 | 381.2 | 856.2 | 52.8 | 10.0 | 28.9 | 2.3 | 5.6 | 0.8 | 5.0 | 0.7 | 64.3 |
|  | 59 | 60 | 1,276 | 23.6\% | 221.6 | 67.4 | 2.3 | 10.5 | 265.1 | 566.9 | 35.7 | 6.1 | 19.6 | 1.7 | 4.4 | 0.6 | 3.9 | 0.6 | 42.4 |
|  | 60 | 61 | 1,459 | 22.8\% | 243.8 | 75.4 | 2.4 | 10.6 | 303.8 | 671.2 | 37.9 | 7.6 | 21.3 | 1.6 | 4.2 | 0.5 | 3.3 | 0.5 | 41.9 |
|  | 61 | 62 | 861 | 21.9\% | 140.0 | 43.0 | 1.0 | 4.5 | 194.7 | 401.8 | 19.9 | 3.2 | 9.7 | 0.7 | 1.7 | 0.2 | 1.4 | 0.3 | 18.8 |


| Hole ID | $\begin{aligned} & \text { From } \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \hline \text { To } \\ & \text { (m) } \end{aligned}$ | TREO (ppm) | $\begin{aligned} & \hline \text { MREO: } \\ & \text { TREO } \end{aligned}$ (\%) | $\begin{aligned} & \mathrm{Nd}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Pr}_{6} \mathrm{O}_{11} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Tb}_{\mathrm{O}} \mathrm{O}_{7} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \hline \mathrm{Dy}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppom}) \end{aligned}$ | $\begin{aligned} & \mathrm{La}_{2} \mathrm{O}_{\mathrm{s}} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{CeO}_{2} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \hline \mathrm{Sm}_{2} \mathrm{O}_{3} \\ & \text { (ppm) } \end{aligned}$ | $\begin{aligned} & \mathrm{E}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{Cd}_{2} \mathrm{O}_{3}$ (ppm) | $\mathrm{HO}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{Er}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Tm}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \mathrm{Yb}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{array} \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \mathrm{L}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{array} \end{aligned}$ | $\begin{gathered} \mathrm{Y}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NEORB002 | 62 | 63 | 855 | 22.9\% | 143.5 | 44.7 | 1.5 | 6.2 | 181.8 | 380.7 | 24.0 | 4.1 | 12.7 | 1.0 | 2.6 | 0.4 | 2.3 | 0.3 | 30.6 |
|  | 63 | 64 | 3,137 | 24.4\% | 562.2 | 174.0 | 5.6 | 24.0 | 382.3 | 1,639.8 | 92.7 | 19.5 | 48.5 | 3.5 | 8.6 | 1.1 | 6.6 | 0.9 | 88.1 |
|  | 64 | 68 | 659 | 22.0\% | 106.3 | 34.0 | 0.9 | 4.0 | 146.6 | 303.4 | 16.0 | 2.8 | 8.4 | 0.6 | 1.6 | 0.2 | 1.4 | 0.2 | 17.9 |
|  | 68 | 69 | 442 | 22.1\% | 72.4 | 22.7 | 0.5 | 2.0 | 102.6 | 205.0 | 10.0 | 2.0 | 4.9 | 0.3 | 0.7 | 0.1 | 0.6 | 0.1 | 7.9 |
|  | 69 | 70 | 760 | 22.0\% | 123.6 | 39.9 | 0.8 | 3.0 | 179.4 | 352.6 | 17.4 | 2.3 | 8.4 | 0.4 | 1.0 | 0.1 | 0.8 | 0.1 | 13.1 |
|  | 70 | 71 | 832 | 24.4\% | 149.3 | 46.9 | 1.3 | 5.2 | 115.4 | 428.7 | 20.6 | 3.7 | 11.5 | 0.8 | 1.9 | 0.3 | 1.5 | 0.2 | 23.9 |
|  | 71 | 72 | 506 | 21.6\% | 80.4 | 23.4 | 1.0 | 4.4 | 109.0 | 227.2 | 14.1 | 3.7 | 9.3 | 0.7 | 1.5 | 0.2 | 1.1 | 0.1 | 19.2 |
|  | 72 | 76 | 261 | 22.1\% | 41.5 | 12.1 | 0.8 | 3.2 | 55.6 | 104.5 | 8.9 | 1.5 | 6.6 | 0.5 | 1.3 | 0.2 | 1.2 | 0.2 | 17.3 |
|  | 76 | 77 | 151 | 21.0\% | 21.2 | 6.5 | 0.6 | 3.3 | 26.7 | 52.9 | 5.3 | 0.7 | 4.6 | 0.6 | 1.7 | 0.3 | 1.5 | 0.2 | 21.7 |
|  | 77 | 78 | 477 | 20.0\% | 66.7 | 21.3 | 1.2 | 6.3 | 104.4 | 188.6 | 12.2 | 2.2 | 10.4 | 1.2 | 3.2 | 0.4 | 2.6 | 0.4 | 46.6 |
| NEORC001 | 0 | 4 | 340 | 22.2\% | 56.0 | 16.6 | 0.6 | 2.3 | 76.5 | 153.4 | 9.1 | 0.9 | 5.1 | 0.4 | 0.8 | 0.1 | 0.6 | 0.1 | 9.7 |
|  | 4 | 5 | 318 | 20.0\% | 46.4 | 15.0 | 0.4 | 1.8 | 69.0 | 157.0 | 7.8 | 0.9 | 4.2 | 0.3 | 0.5 | 0.1 | 0.3 | 0.1 | 6.7 |
|  | 5 | 6 | 560 | 21.7\% | 89.3 | 27.7 | 0.9 | 3.8 | 126.7 | 256.5 | 15.1 | 1.2 | 8.3 | 0.6 | 1.3 | 0.1 | 0.8 | 0.1 | 15.4 |
|  | 6 | 7 | 540 | 21.3\% | 85.1 | 25.6 | 0.9 | 3.4 | 123.1 | 249.5 | 14.0 | 1.1 | 7.8 | 0.5 | 1.3 | 0.1 | 0.9 | 0.1 | 14.5 |
|  | 7 | 8 | 755 | 21.9\% | 122.5 | 37.5 | 1.1 | 4.0 | 168.9 | 353.7 | 19.8 | 1.4 | 10.2 | 0.6 | 1.4 | 0.2 | 1.0 | 0.2 | 15.4 |
|  | 8 | 9 | 945 | 21.3\% | 149.3 | 46.5 | 1.2 | 4.7 | 218.1 | 445.1 | 24.2 | 1.7 | 12.2 | 0.6 | 1.4 | 0.2 | 1.1 | 0.2 | 16.8 |
|  | 9 | 10 | 649 | 22.0\% | 106.4 | 32.6 | 0.8 | 2.9 | 151.3 | 301.0 | 17.2 | 1.2 | 8.4 | 0.4 | 0.9 | 0.1 | 0.6 | 0.1 | 10.6 |
|  | 10 | 11 | 409 | 22.2\% | 67.3 | 21.0 | 0.6 | 2.2 | 91.9 | 188.6 | 11.7 | 1.1 | 6.0 | 0.3 | 0.8 | 0.1 | 0.5 | 0.1 | 8.1 |
|  | 11 | 12 | 523 | 21.2\% | 82.2 | 26.2 | 0.6 | 2.0 | 123.1 | 247.1 | 12.8 | 1.3 | 6.0 | 0.3 | 0.6 | 0.1 | 0.5 | 0.1 | 7.8 |
|  | 12 | 13 | 426 | 21.1\% | 67.1 | 20.5 | 0.5 | 1.7 | 102.6 | 197.9 | 10.4 | 1.2 | 5.0 | 0.3 | 0.7 | 0.1 | 0.5 | 0.1 | 7.8 |
|  | 13 | 14 | 444 | 21.5\% | 71.4 | 22.5 | 0.4 | 1.5 | 106.0 | 209.7 | 10.4 | 1.1 | 4.7 | 0.2 | 0.4 | 0.1 | 0.3 | 0.0 | 5.5 |
|  | 14 | 15 | 460 | 20.8\% | 70.7 | 22.8 | 0.5 | 1.6 | 111.3 | 217.9 | 10.5 | 1.1 | 4.7 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 6.9 |
|  | 15 | 16 | 282 | 21.6\% | 45.1 | 14.1 | 0.4 | 1.3 | 65.1 | 131.2 | 7.8 | 0.6 | 3.9 | 0.2 | 0.4 | 0.0 | 0.2 | 0.0 | 5.3 |
|  | 16 | 17 | 418 | 20.2\% | 62.2 | 20.5 | 0.4 | 1.5 | 103.6 | 197.9 | 9.4 | 1.0 | 4.3 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 6.4 |
|  | 17 | 18 | 492 | 19.9\% | 71.9 | 23.9 | 0.5 | 1.7 | 123.1 | 233.1 | 11.2 | 1.1 | 5.0 | 0.3 | 0.6 | 0.1 | 0.5 | 0.1 | 7.4 |
|  | 18 | 19 | 831 | 21.1\% | 130.6 | 42.3 | 0.7 | 1.9 | 199.4 | 400.6 | 18.7 | 1.5 | 7.7 | 0.3 | 0.5 | 0.1 | 0.3 | 0.0 | 6.5 |
|  | 19 | 20 | 421 | 20.6\% | 64.0 | 21.3 | 0.3 | 1.1 | 104.4 | 201.5 | 9.1 | 1.1 | 3.8 | 0.1 | 0.3 | 0.0 | 0.1 | 0.0 | 3.7 |
|  | 20 | 21 | 955 | 21.6\% | 154.0 | 48.3 | 0.8 | 2.8 | 225.2 | 455.6 | 22.5 | 2.0 | 9.2 | 0.4 | 0.9 | 0.1 | 0.5 | 0.1 | 10.5 |
|  | 21 | 22 | 680 | 21.6\% | 110.3 | 33.7 | 0.6 | 1.9 | 160.7 | 324.5 | 16.2 | 1.3 | 7.1 | 0.3 | 0.5 | 0.1 | 0.3 | 0.1 | 6.7 |
|  | 22 | 23 | 945 | 21.4\% | 150.5 | 48.3 | 0.8 | 2.4 | 221.7 | 453.3 | 22.0 | 2.2 | 9.5 | 0.3 | 0.8 | 0.1 | 0.6 | 0.1 | 10.3 |
|  | 23 | 24 | 845 | 21.7\% | 137.6 | 43.1 | 0.7 | 2.1 | 198.2 | 404.1 | 20.2 | 1.7 | 8.0 | 0.3 | 0.5 | 0.1 | 0.5 | 0.1 | 7.9 |
|  | 24 | 28 | 691 | 21.7\% | 112.0 | 35.2 | 0.6 | 2.1 | 163.0 | 328.0 | 16.8 | 1.8 | 7.2 | 0.2 | 0.6 | 0.1 | 0.4 | 0.1 | 7.0 |
|  | 28 | 32 | 662 | 21.1\% | 104.3 | 32.9 | 0.7 | 2.2 | 159.5 | 313.9 | 15.4 | 2.0 | 6.9 | 0.3 | 0.7 | 0.1 | 0.4 | 0.1 | 7.6 |
|  | 32 | 36 | 488 | 21.3\% | 77.2 | 24.3 | 0.5 | 1.7 | 116.3 | 229.6 | 11.3 | 1.6 | 5.5 | 0.3 | 0.5 | 0.1 | 0.4 | 0.1 | 7.0 |
|  | 36 | 37 | 689 | 22.0\% | 112.7 | 35.0 | 0.9 | 3.1 | 152.5 | 322.1 | 18.2 | 4.0 | 8.7 | 0.5 | 1.1 | 0.1 | 0.8 | 0.1 | 13.7 |
|  | 37 | 38 | 538 | 22.0\% | 88.2 | 27.3 | 0.6 | 2.1 | 120.8 | 255.3 | 13.7 | 2.9 | 6.0 | 0.3 | 0.7 | 0.1 | 0.5 | 0.1 | 7.3 |
|  | 38 | 39 | 940 | 21.9\% | 155.1 | 47.4 | 0.8 | 2.7 | 218.1 | 445.1 | 23.2 | 3.5 | 9.9 | 0.4 | 0.9 | 0.1 | 0.6 | 0.1 | 10.3 |
|  | 39 | 40 | 532 | 21.9\% | 87.2 | 26.7 | 0.6 | 2.1 | 119.6 | 250.7 | 13.5 | 2.9 | 6.0 | 0.3 | 0.7 | 0.1 | 0.6 | 0.1 | 8.6 |
| NEORB003 | 0 | 4 | 313 | 21.2\% | 48.1 | 14.1 | 0.7 | 3.4 | 63.8 | 146.2 | 8.0 | 1.8 | 5.5 | 0.6 | 1.5 | 0.2 | 1.5 | 0.2 | 17.1 |
|  | 4 | 5 | 1,245 | 21.4\% | 194.8 | 58.8 | 2.2 | 10.7 | 286.2 | 573.7 | 29.2 | 6.6 | 17.4 | 1.8 | 4.4 | 0.6 | 3.4 | 0.5 | 55.2 |
|  | 5 |  | 1,445 | 22.0\% | 232.1 | 69.0 | 3.0 | 14.0 | 319.0 | 651.1 | 36.4 | 8.9 | 23.2 | 2.3 | 5.9 | 0.7 | 4.4 | 0.6 | 74.7 |
|  | 6 | 7 | 704 | 20.2\% | 102.8 | 31.2 | 1.5 | 7.1 | 156.0 | 330.4 | 16.1 | 3.6 | 11.0 | 1.2 | 3.1 | 0.4 | 2.6 | 0.4 | 36.4 |
|  | 7 | 8 | 351 | 20.3\% | 51.6 | 15.2 | 0.8 | 3.7 | 67.9 | 172.0 | 9.0 | 2.2 | 6.0 | 0.6 | 1.6 | 0.2 | 1.5 | 0.2 | 18.8 |
|  | 8 | 9 | 653 | 21.4\% | 100.9 | 28.9 | 1.8 | 8.6 | 139.6 | 287.4 | 17.6 | 4.1 | 12.7 | 1.4 | 3.6 | 0.5 | 2.9 | 0.4 | 42.8 |
|  | 9 | 10 | 729 | 20.8\% | 109.9 | 33.2 | 1.5 | 6.8 | 153.6 | 353.8 | 19.2 | 3.9 | 11.1 | 1.1 | 2.8 | 0.4 | 2.3 | 0.3 | 29.5 |
|  | 10 | 11 | 541 | 20.2\% | 78.1 | 23.3 | 1.3 | 6.6 | 112.6 | 254.3 | 13.3 | 2.8 | 9.3 | 1.1 | 2.7 | 0.4 | 2.2 | 0.3 | 33.0 |
|  | 11 | 12 | 1,493 | 20.2\% | 215.8 | 69.6 | 2.8 | 13.2 | 336.6 | 713.7 | 34.8 | 6.5 | 20.6 | 2.1 | 5.4 | 0.7 | 4.3 | 0.6 | 66.4 |
|  | 12 | 13 | 1,705 | 19.8\% | 243.8 | 77.2 | 2.9 | 13.3 | 412.8 | 805.8 | 36.2 | 5.7 | 21.2 | 2.3 | 5.9 | 0.8 | 5.2 | 0.7 | 71.2 |
|  | 13 | 14 | 489 | 20.2\% | 72.3 | 22.2 | 0.7 | 3.6 | 112.0 | 238.3 | 11.2 | 1.5 | 6.1 | 0.6 | 1.5 | 0.2 | 1.5 | 0.2 | 17.3 |
|  | 14 | 15 | 381 | 19.6\% | 54.8 | 17.0 | 0.5 | 2.2 | 87.4 | 191.6 | 8.5 | 1.3 | 4.3 | 0.4 | 1.0 | 0.1 | 1.0 | 0.1 | 10.9 |
|  | 15 | 16 | 193 | 20.4\% | 28.7 | 8.8 | 0.3 | 1.5 | 42.3 | 92.6 | 4.5 | 0.8 | 2.5 | 0.3 | 0.8 | 0.1 | 0.8 | 0.1 | 8.7 |
|  | 16 | 20 | 760 | 19.7\% | 110.8 | 34.2 | 0.9 | 4.1 | 178.3 | 379.6 | 16.8 | 2.1 | 8.2 | 0.6 | 1.6 | 0.2 | 1.4 | 0.2 | 20.8 |
|  | 20 | 24 | 416 | 20.2\% | 61.8 | 19.1 | 0.6 | 2.7 | 96.2 | 203.9 | 9.7 | 1.7 | 5.1 | 0.4 | 1.0 | 0.1 | 0.8 | 0.1 | 12.5 |
|  | 24 | 25 | 282 | 19.5\% | 40.2 | 12.7 | 0.4 | 1.8 | 66.4 | 138.8 | 6.2 | 1.5 | 3.3 | 0.3 | 0.7 | 0.1 | 0.7 | 0.1 | 9.3 |
|  | 25 | 26 | 205 | 20.2\% | 29.9 | 9.3 | 0.4 | 1.9 | 45.7 | 97.0 | 5.4 | 1.0 | 3.0 | 0.3 | 0.8 | 0.1 | 0.8 | 0.1 | 9.1 |
|  | 26 | 27 | 275 | 20.4\% | 40.6 | 12.2 | 0.6 | 2.8 | 60.4 | 127.8 | 7.1 | 1.2 | 4.1 | 0.5 | 1.3 | 0.2 | 1.3 | 0.2 | 14.5 |


| Hole ID | From (m) | $\begin{aligned} & \hline \text { To } \\ & \text { (m) } \end{aligned}$ | TREO (ppm) | $\begin{gathered} \hline \text { MREO: } \\ \text { TREO } \\ (\%) \\ \hline \hline \end{gathered}$ | $\mathrm{Nd}_{2} \mathrm{O}_{3}$ (ppm) | $\mathrm{Pr}_{6} \mathrm{O}_{11}$ (ppm) | $\mathrm{Tb}_{4} \mathrm{O}_{7}$ (ppm) | $\begin{aligned} & \hline \mathrm{Dy}_{2} \mathrm{O}_{\mathrm{s}} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \hline \mathrm{La}_{2} \mathrm{O}_{8} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{CeO}_{2}$ (ppm) | $\mathrm{Sm}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{Eu}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{Cd}_{2} \mathrm{O}_{3}$ (ppm) | $\mathrm{HO}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{Er}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{Tm}_{2} \mathrm{O}_{3}$ (ppm) | $\mathrm{Yb}_{2} \mathrm{O}_{3}$ (ppm) | $\mathrm{Lu}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{gathered} \mathrm{Y}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 27 | 28 | 1,169 | 20.5\% | 173.8 | 51.2 | 2.4 | 11.9 | 267.4 | 523.3 | 29.3 | 6.4 | 18.7 | 2.1 | 5.7 | 0.8 | 5.3 | 0.8 | 69.5 |
|  | 28 | 29 | 1,774 | 20.0\% | 257.8 | 79.5 | 3.0 | 14.5 | 422.2 | 809.5 | 40.8 | 7.9 | 23.5 | 2.6 | 7.1 | 1.0 | 6.8 | 1.0 | 96.8 |
|  | 29 | 30 | 273 | 20.3\% | 40.1 | 12.0 | 0.6 | 2.7 | 61.2 | 125.3 | 7.1 | 1.4 | 4.7 | 0.5 | 1.3 | 0.2 | 1.2 | 0.2 | 14.2 |
|  | 30 | 31 | 1,977 | 20.5\% | 291.6 | 83.0 | 5.2 | 25.7 | 472.6 | 825.5 | 52.0 | 13.4 | 39.3 | 4.6 | 12.0 | 1.6 | 10.6 | 1.5 | 138.4 |
|  | 31 | 32 | 563 | 20.0\% | 83.5 | 25.4 | 0.9 | 3.1 | 137.2 | 273.9 | 12.5 | 2.8 | 6.4 | 0.5 | 1.2 | 0.2 | 1.0 | 0.1 | 14.2 |
|  | 32 | 33 | 334 | 19.8\% | 48.8 | 14.9 | 0.5 | 2.2 | 81.9 | 159.7 | 8.0 | 1.7 | 4.3 | 0.4 | 0.9 | 0.1 | 0.9 | 0.1 | 10.2 |
|  | 33 | 34 | 497 | 20.0\% | 73.5 | 22.8 | 0.6 | 2.4 | 119.6 | 245.7 | 10.9 | 2.5 | 5.2 | 0.4 | 0.9 | 0.1 | 0.8 | 0.1 | 11.1 |
|  | 34 | 35 | 462 | 20.0\% | 68.7 | 20.5 | 0.6 | 2.3 | 111.1 | 227.3 | 10.3 | 2.2 | 4.9 | 0.4 | 0.9 | 0.1 | 0.9 | 0.1 | 11.3 |
|  | 35 | 36 | 825 | 19.9\% | 122.5 | 36.9 | 0.9 | 3.9 | 195.9 | 410.3 | 17.6 | 2.9 | 8.4 | 0.6 | 1.7 | 0.3 | 1.7 | 0.3 | 21.3 |
|  | 36 | 40 | 615 | 20.0\% | 91.0 | 28.4 | 0.7 | 3.0 | 146.6 | 304.6 | 13.9 | 2.0 | 6.4 | 0.5 | 1.3 | 0.2 | 1.2 | 0.2 | 15.4 |
|  | 40 | 44 | 505 | 20.1\% | 75.1 | 23.0 | 0.7 | 3.0 | 115.2 | 250.6 | 11.4 | 1.5 | 5.4 | 0.5 | 1.3 | 0.2 | 1.3 | 0.2 | 15.9 |
|  | 44 | 45 | 369 | 20.2\% | 54.4 | 17.2 | 0.6 | 2.7 | 84.1 | 180.6 | 8.4 | 1.1 | 4.9 | 0.4 | 1.1 | 0.2 | 1.1 | 0.2 | 12.6 |
|  | 45 | 46 | 540 | 19.9\% | 78.3 | 23.9 | 0.9 | 4.3 | 123.1 | 260.4 | 12.6 | 1.8 | 7.2 | 0.7 | 1.9 | 0.3 | 1.9 | 0.3 | 22.6 |
|  | 46 | 47 | 801 | 21.6\% | 129.5 | 40.1 | 0.8 | 2.9 | 190.0 | 393.1 | 20.1 | 1.3 | 9.6 | 0.4 | 0.9 | 0.1 | 0.7 | 0.1 | 11.7 |
|  | 47 | 48 | 795 | 20.2\% | 115.4 | 33.5 | 2.1 | 9.9 | 180.6 | 355.0 | 20.8 | 4.3 | 15.6 | 1.7 | 4.1 | 0.6 | 3.3 | 0.5 | 48.1 |
|  | 48 | 49 | 430 | 21.5\% | 66.6 | 19.8 | 1.1 | 5.0 | 90.1 | 194.1 | 12.4 | 2.7 | 7.7 | 0.8 | 2.2 | 0.3 | 1.8 | 0.2 | 25.5 |
|  | 49 | 50 | 338 | 21.9\% | 54.0 | 16.8 | 0.6 | 2.6 | 72.0 | 159.7 | 9.0 | 1.6 | 5.0 | 0.5 | 1.2 | 0.2 | 1.0 | 0.1 | 13.6 |
|  | 50 | 51 | 248 | 22.0\% | 39.9 | 11.8 | 0.5 | 2.4 | 50.9 | 114.5 | 7.2 | 1.5 | 4.2 | 0.4 | 1.1 | 0.2 | 1.1 | 0.2 | 12.6 |
|  | 51 | 52 | 458 | 20.7\% | 70.1 | 21.9 | 0.5 | 2.3 | 106.4 | 226.0 | 9.8 | 2.5 | 4.8 | 0.4 | 1.0 | 0.1 | 0.9 | 0.1 | 10.9 |
|  | 52 | 53 | 772 | 20.8\% | 119.0 | 37.3 | 0.8 | 3.1 | 183.0 | 379.6 | 17.4 | 2.9 | 7.7 | 0.5 | 1.5 | 0.2 | 1.5 | 0.2 | 16.9 |
|  | 53 | 54 | 2,046 | 21.5\% | 325.4 | 104.3 | 2.0 | 7.7 | 479.7 | 1,004.8 | 46.7 | 4.9 | 20.6 | 1.3 | 3.6 | 0.5 | 3.4 | 0.5 | 41.0 |
|  | 54 | 55 | 744 | 21.1\% | 116.3 | 36.5 | 0.8 | 3.4 | 175.9 | 361.1 | 17.2 | 3.1 | 8.1 | 0.6 | 1.5 | 0.2 | 1.4 | 0.2 | 17.7 |
|  | 55 | 56 | 344 | 20.4\% | 51.2 | 16.2 | 0.5 | 2.3 | 82.2 | 162.1 | 8.1 | 2.7 | 4.7 | 0.4 | 0.9 | 0.1 | 0.9 | 0.1 | 11.6 |
|  | 56 | 57 | 426 | 21.6\% | 67.7 | 20.3 | 0.7 | 3.3 | 95.2 | 199.0 | 11.0 | 2.4 | 6.1 | 0.5 | 1.5 | 0.2 | 1.3 | 0.2 | 16.9 |
|  | 57 | 58 | 543 | 21.7\% | 86.9 | 26.6 | 0.8 | 3.4 | 125.5 | 255.5 | 13.1 | 3.0 | 6.8 | 0.6 | 1.5 | 0.2 | 1.4 | 0.2 | 17.9 |
|  | 58 | 59 | 797 | 21.1\% | 122.5 | 38.3 | 1.3 | 6.6 | 173.6 | 372.2 | 19.5 | 3.0 | 10.6 | 1.3 | 4.2 | 0.7 | 5.4 | 0.9 | 37.5 |
|  | 59 | 60 | 420 | 21.5\% | 65.9 | 20.2 | 0.8 | 3.5 | 92.7 | 196.5 | 10.8 | 1.8 | 6.3 | 0.6 | 1.7 | 0.2 | 1.7 | 0.2 | 17.3 |
|  | 60 | 61 | 968 | 20.3\% | 142.3 | 45.7 | 1.6 | 7.2 | 231.0 | 458.2 | 22.5 | 3.5 | 13.0 | 1.2 | 3.0 | 0.4 | 2.8 | 0.4 | 34.9 |
|  | 61 | 62 | 576 | 20.2\% | 84.2 | 26.5 | 1.0 | 4.9 | 137.2 | 270.2 | 13.7 | 2.0 | 8.2 | 0.8 | 2.1 | 0.3 | 1.8 | 0.3 | 22.6 |
|  | 62 | 63 | 343 | 20.3\% | 50.6 | 15.3 | 0.7 | 3.2 | 81.3 | 158.5 | 8.3 | 1.3 | 5.5 | 0.5 | 1.5 | 0.2 | 1.3 | 0.2 | 14.7 |
|  | 63 | 64 | 1,037 | 22.2\% | 168.0 | 51.2 | 2.0 | 8.6 | 232.2 | 476.6 | 27.6 | 3.1 | 15.8 | 1.5 | 3.9 | 0.5 | 3.6 | 0.5 | 41.7 |
|  | 64 | 65 | 946 | 21.6\% | 149.3 | 45.8 | 1.6 | 7.5 | 215.8 | 439.8 | 23.2 | 3.0 | 13.3 | 1.3 | 3.7 | 0.5 | 3.5 | 0.5 | 37.3 |
|  | 65 | 66 | 569 | 21.1\% | 87.8 | 27.5 | 0.9 | 4.1 | 132.5 | 267.8 | 14.1 | 2.7 | 7.8 | 0.7 | 1.8 | 0.3 | 1.6 | 0.2 | 19.3 |
|  | 66 | 67 | 454 | 22.1\% | 73.9 | 22.6 | 0.7 | 3.1 | 103.8 | 212.5 | 12.1 | 2.0 | 6.5 | 0.5 | 1.3 | 0.2 | 1.1 | 0.2 | 13.8 |
|  | 67 | 68 | 538 | 21.6\% | 85.8 | 25.0 | 1.0 | 4.4 | 124.3 | 244.5 | 14.4 | 3.6 | 8.3 | 0.7 | 1.8 | 0.3 | 1.7 | 0.2 | 21.5 |
|  | 68 | 72 | 665 | 21.7\% | 107.1 | 31.3 | 1.2 | 5.0 | 159.5 | 299.7 | 17.2 | 3.9 | 10.4 | 0.8 | 2.1 | 0.3 | 1.6 | 0.2 | 24.4 |
|  | 72 | 73 | 330 | 20.9\% | 51.1 | 14.9 | 0.5 | 2.5 | 81.0 | 148.6 | 8.0 | 2.4 | 5.0 | 0.4 | 1.1 | 0.1 | 0.9 | 0.1 | 13.7 |
|  | 73 | 74 | 575 | 20.4\% | 86.5 | 26.3 | 0.8 | 3.8 | 138.4 | 266.6 | 14.0 | 2.7 | 8.0 | 0.6 | 1.8 | 0.2 | 1.7 | 0.2 | 23.0 |
|  | 74 | 75 | 584 | 21.2\% | 91.9 | 28.5 | 0.8 | 2.9 | 136.0 | 280.1 | 14.7 | 2.0 | 7.2 | 0.5 | 1.2 | 0.2 | 1.1 | 0.1 | 17.1 |
|  | 75 | 76 | 732 | 20.5\% | 110.0 | 34.9 | 1.0 | 4.0 | 177.1 | 348.9 | 17.4 | 2.4 | 9.5 | 0.7 | 1.8 | 0.2 | 1.5 | 0.2 | 22.9 |
|  | 76 | 77 | 779 | 20.5\% | 117.8 | 36.7 | 1.0 | 4.2 | 188.8 | 374.7 | 18.0 | 2.2 | 9.8 | 0.7 | 1.7 | 0.2 | 1.3 | 0.2 | 21.3 |
|  | 77 | 78 | 1,410 | 21.0\% | 218.1 | 69.1 | 1.6 | 6.6 | 342.5 | 667.0 | 33.4 | 3.0 | 17.2 | 1.2 | 3.1 | 0.4 | 2.6 | 0.4 | 43.9 |
| NEORB004 | 0 | 4 | 455 | 21.8\% | 73.2 | 22.2 | 0.7 | 3.0 | 103.7 | 215.0 | 11.2 | 1.6 | 5.9 | 0.5 | 1.2 | 0.2 | 1.1 | 0.1 | 15.7 |
|  | 4 | 8 | 621 | 20.9\% | 95.6 | 30.7 | 0.7 | 2.7 | 144.3 | 308.3 | 15.0 | 2.1 | 6.8 | 0.4 | 1.0 | 0.1 | 0.9 | 0.1 | 12.3 |
|  | 8 | 9 | 419 | 20.3\% | 62.5 | 20.2 | 0.5 | 2.1 | 98.3 | 208.8 | 9.9 | 1.1 | 5.0 | 0.3 | 0.8 | 0.1 | 0.5 | 0.1 | 9.1 |
|  | 9 | 10 | 406 | 20.4\% | 60.9 | 19.3 | 0.5 | 2.1 | 95.2 | 201.5 | 9.6 | 1.2 | 4.8 | 0.3 | 0.8 | 0.1 | 0.6 | 0.1 | 9.4 |
|  | 10 | 11 | 537 | 20.2\% | 80.2 | 26.2 | 0.5 | 1.8 | 130.2 | 270.2 | 12.1 | 1.4 | 5.3 | 0.2 | 0.6 | 0.1 | 0.4 | 0.1 | 7.7 |
|  | 11 | 12 | 412 | 20.7\% | 63.7 | 20.2 | 0.3 | 1.1 | 99.5 | 206.4 | 9.6 | 1.2 | 3.9 | 0.2 | 0.4 | 0.0 | 0.3 | 0.0 | 5.2 |
|  | 12 | 13 | 465 | 20.8\% | 71.9 | 23.0 | 0.4 | 1.6 | 109.2 | 234.6 | 10.4 | 1.2 | 5.0 | 0.2 | 0.6 | 0.1 | 0.3 | 0.1 | 6.5 |
|  | 13 | 14 | 648 | 21.1\% | 101.6 | 32.7 | 0.6 | 1.8 | 154.8 | 325.5 | 14.3 | 1.5 | 6.2 | 0.3 | 0.7 | 0.1 | 0.4 | 0.1 | 7.9 |
|  | 14 | 15 | 269 | 21.1\% | 42.3 | 13.3 | 0.2 | 0.7 | 64.2 | 135.1 | 5.9 | 0.7 | 2.6 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 3.1 |
|  | 15 | 16 | 503 | 21.0\% | 77.9 | 24.9 | 0.6 | 2.2 | 117.3 | 250.6 | 12.1 | 1.1 | 5.9 | 0.3 | 0.7 | 0.1 | 0.5 | 0.1 | 8.5 |
|  | 16 | 20 | 372 | 21.1\% | 58.6 | 18.5 | 0.4 | 1.3 | 88.8 | 185.5 | 8.5 | 0.8 | 3.9 | 0.2 | 0.4 | 0.0 | 0.3 | 0.0 | 5.2 |
|  | 20 | 24 | 374 | 21.0\% | 58.1 | 18.7 | 0.4 | 1.3 | 89.4 | 185.5 | 9.0 | 0.9 | 4.3 | 0.2 | 0.4 | 0.0 | 0.3 | 0.0 | 5.0 |
|  | 24 | 25 | 653 | 21.5\% | 105.0 | 33.2 | 0.6 | 1.8 | 157.2 | 324.3 | 15.1 | 1.0 | 7.0 | 0.3 | 0.5 | 0.1 | 0.4 | 0.1 | 6.8 |
|  | 25 | 26 | 283 | 21.3\% | 45.1 | 13.9 | 0.3 | 0.9 | 67.7 | 140.0 | 6.5 | 0.7 | 3.1 | 0.1 | 0.3 | 0.0 | 0.2 | 0.0 | 4.0 |
|  | 26 | 27 | 201 | 19.9\% | 29.6 | 9.6 | 0.2 | 0.7 | 50.3 | 99.9 | 4.6 | 0.7 | 2.2 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 2.7 |


| Hole ID | From (m) | To <br> (m) | $\begin{aligned} & \text { TREO } \\ & \text { (ppm) } \end{aligned}$ | $\begin{aligned} & \text { MREO: } \\ & \text { TREO } \end{aligned}$ $(\%)$ | $\begin{aligned} & \mathrm{Nd}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Pr}_{\mathrm{r}} \mathrm{O}_{11} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{Tb}_{4} \mathrm{O}_{7}$ (ppm) | $\begin{aligned} & \mathrm{Dy}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{La}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{gathered} \mathrm{CeO}_{2} \\ (\mathrm{ppm}) \end{gathered}$ | $\begin{aligned} & \mathrm{Sm}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Eu}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Gd}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Ho}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Er}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Tm}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Yb}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Lu}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{gathered} \mathbf{Y}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 27 | 28 | 760 | 21.4\% | 120.1 | 38.2 | 1.0 | 3.3 | 167.7 | 382.0 | 19.7 | 1.5 | 10.1 | 0.5 | 1.1 | 0.1 | 1.0 | 0.2 | 13.2 |
|  | 28 | 29 | 521 | 21.9\% | 84.8 | 26.7 | 0.6 | 1.9 | 116.2 | 261.6 | 14.4 | 1.0 | 6.8 | 0.3 | 0.5 | 0.0 | 0.3 | 0.0 | 6.0 |
|  | 29 | 30 | 956 | 21.4\% | 152.8 | 48.6 | 0.8 | 2.2 | 229.9 | 479.1 | 21.7 | 1.4 | 10.1 | 0.3 | 0.7 | 0.1 | 0.4 | 0.1 | 8.0 |
|  | 30 | 31 | 888 | 21.5\% | 143.5 | 44.9 | 0.7 | 2.0 | 209.9 | 449.6 | 19.9 | 1.6 | 8.5 | 0.2 | 0.5 | 0.1 | 0.3 | 0.1 | 6.7 |
|  | 31 | 32 | 978 | 22.2\% | 162.1 | 51.6 | 0.8 | 2.2 | 239.3 | 477.8 | 23.0 | 1.3 | 10.0 | 0.3 | 0.7 | 0.1 | 0.5 | 0.1 | 8.6 |
|  | 32 | 33 | 695 | 21.3\% | 111.0 | 34.9 | 0.6 | 1.6 | 166.5 | 348.9 | 15.9 | 1.2 | 6.9 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 6.4 |
|  | 33 | 34 | 432 | 21.1\% | 68.2 | 21.5 | 0.4 | 1.1 | 105.8 | 215.0 | 9.9 | 1.0 | 4.4 | 0.1 | 0.3 | 0.0 | 0.2 | 0.0 | 4.0 |
|  | 34 | 35 | 637 | 21.1\% | 99.7 | 31.9 | 0.6 | 1.9 | 152.5 | 319.4 | 14.6 | 1.3 | 6.8 | 0.2 | 0.5 | 0.1 | 0.3 | 0.0 | 6.8 |
|  | 35 | 36 | 207 | 20.9\% | 32.3 | 10.1 | 0.2 | 0.7 | 50.8 | 102.0 | 4.8 | 0.7 | 2.3 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 2.7 |
|  | 36 | 40 | 310 | 21.5\% | 49.8 | 15.5 | 0.3 | 1.2 | 71.8 | 154.8 | 7.0 | 1.2 | 3.4 | 0.2 | 0.4 | 0.0 | 0.2 | 0.0 | 4.4 |
|  | 40 | 44 | 393 | 20.8\% | 60.5 | 19.5 | 0.4 | 1.4 | 93.8 | 195.3 | 8.8 | 1.7 | 4.3 | 0.2 | 0.5 | 0.0 | 0.3 | 0.0 | 5.8 |
|  | 44 | 45 | 333 | 20.9\% | 51.9 | 16.4 | 0.3 | 1.1 | 81.2 | 163.4 | 7.5 | 1.7 | 3.5 | 0.2 | 0.4 | 0.0 | 0.3 | 0.0 | 5.2 |
|  | 45 | 46 | 273 | 21.2\% | 43.0 | 13.7 | 0.3 | 0.9 | 64.6 | 135.1 | 6.4 | 1.1 | 2.9 | 0.1 | 0.4 | 0.0 | 0.3 | 0.0 | 4.2 |
|  | 46 | 47 | 767 | 21.6\% | 123.6 | 38.5 | 0.8 | 3.1 | 178.3 | 378.3 | 18.9 | 1.4 | 9.4 | 0.4 | 1.0 | 0.1 | 0.8 | 0.1 | 12.3 |
|  | 47 | 48 | 986 | 22.1\% | 163.3 | 50.1 | 1.1 | 3.8 | 224.0 | 485.2 | 25.0 | 2.8 | 11.8 | 0.6 | 1.3 | 0.2 | 1.0 | 0.1 | 15.9 |
|  | 48 | 49 | 591 | 22.2\% | 97.7 | 29.7 | 0.8 | 3.1 | 129.0 | 288.7 | 14.7 | 3.8 | 7.5 | 0.5 | 1.3 | 0.2 | 1.2 | 0.2 | 12.5 |
|  | 49 | 50 | 556 | 22.2\% | 92.1 | 28.0 | 0.7 | 2.6 | 122.0 | 272.7 | 14.0 | 3.4 | 6.8 | 0.4 | 1.1 | 0.2 | 1.0 | 0.2 | 11.3 |
|  | 50 | 51 | 531 | 21.5\% | 84.0 | 26.7 | 0.7 | 2.9 | 118.5 | 259.2 | 13.3 | 3.3 | 6.7 | 0.4 | 1.3 | 0.2 | 1.1 | 0.2 | 13.1 |
|  | 51 | 52 | 765 | 22.5\% | 128.3 | 39.1 | 1.0 | 4.0 | 168.9 | 364.8 | 20.2 | 6.5 | 10.5 | 0.7 | 1.8 | 0.2 | 1.6 | 0.2 | 17.4 |
|  | 52 | 53 | 554 | 22.3\% | 91.7 | 27.8 | 0.7 | 3.1 | 120.8 | 266.6 | 15.0 | 4.5 | 7.7 | 0.5 | 1.2 | 0.2 | 0.9 | 0.1 | 13.0 |
|  | 53 | 54 | 561 | 21.7\% | 89.6 | 28.9 | 0.7 | 2.7 | 130.2 | 271.5 | 13.9 | 3.5 | 6.7 | 0.4 | 1.1 | 0.1 | 1.0 | 0.1 | 10.8 |
|  | 54 | 55 | 440 | 21.5\% | 70.3 | 21.7 | 0.6 | 2.1 | 104.6 | 211.3 | 11.3 | 2.0 | 6.0 | 0.3 | 0.8 | 0.1 | 0.8 | 0.1 | 8.4 |
|  | 55 | 56 | 427 | 21.5\% | 68.5 | 21.1 | 0.4 | 1.6 | 101.7 | 208.8 | 10.5 | 2.0 | 5.0 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 6.2 |
|  | 56 | 60 | 418 | 21.5\% | 67.1 | 20.5 | 0.5 | 1.8 | 101.1 | 201.5 | 10.3 | 1.6 | 5.3 | 0.3 | 0.6 | 0.1 | 0.4 | 0.1 | 7.1 |
|  | 60 | 64 | 157 | 21.1\% | 24.7 | 7.5 | 0.2 | 0.6 | 36.7 | 76.8 | 3.6 | 0.8 | 1.9 | 0.1 | 0.3 | 0.0 | 0.1 | 0.0 | 3.4 |
|  | 64 | 65 | 205 | 21.3\% | 32.0 | 9.6 | 0.4 | 1.8 | 42.8 | 94.5 | 5.3 | 1.4 | 3.2 | 0.4 | 1.0 | 0.1 | 0.8 | 0.1 | 12.1 |
|  | 65 | 66 | 59 | 20.1\% | 8.3 | 2.2 | 0.2 | 1.2 | 10.6 | 20.1 | 1.7 | 0.8 | 1.5 | 0.3 | 0.8 | 0.1 | 0.6 | 0.1 | 10.4 |
|  | 66 | 67 | 434 | 20.4\% | 65.0 | 20.1 | 0.7 | 3.0 | 101.8 | 201.5 | 9.9 | 2.7 | 5.9 | 0.5 | 1.5 | 0.2 | 1.0 | 0.2 | 20.7 |
|  | 67 | 68 | 2,045 | 17.5\% | 239.1 | 56.5 | 10.1 | 52.6 | 445.7 | 536.8 | 47.7 | 26.1 | 77.0 | 10.8 | 29.3 | 3.2 | 17.4 | 3.0 | 490.2 |
|  | 68 | 69 | 363 | 20.6\% | 51.9 | 13.7 | 1.6 | 7.8 | 67.8 | 132.7 | 11.7 | 3.7 | 11.1 | 1.4 | 3.6 | 0.5 | 2.7 | 0.5 | 52.4 |
|  | 69 | 70 | 281 | 21.1\% | 43.4 | 12.9 | 0.5 | 2.3 | 60.8 | 130.2 | 7.0 | 1.7 | 4.3 | 0.4 | 1.1 | 0.1 | 0.8 | 0.1 | 14.9 |
|  | 70 | 71 | 258 | 21.1\% | 40.8 | 12.4 | 0.3 | 0.9 | 59.8 | 127.8 | 6.0 | 1.1 | 2.8 | 0.1 | 0.4 | 0.0 | 0.2 | 0.0 | 5.5 |
|  | 71 | 72 | 411 | 21.6\% | 66.3 | 20.2 | 0.5 | 1.7 | 93.0 | 201.5 | 10.2 | 1.7 | 5.2 | 0.3 | 0.6 | 0.1 | 0.4 | 0.1 | 9.5 |
|  | 72 | 73 | 427 | 21.1\% | 67.1 | 20.5 | 0.6 | 2.0 | 95.5 | 208.8 | 11.1 | 2.7 | 5.7 | 0.3 | 0.7 | 0.1 | 0.5 | 0.1 | 11.2 |
|  | 73 | 74 | 581 | 22.3\% | 97.0 | 26.7 | 1.1 | 4.5 | 130.2 | 262.9 | 15.9 | 3.8 | 9.9 | 0.7 | 1.6 | 0.2 | 1.0 | 0.2 | 24.9 |
|  | 74 | 75 | 621 | 24.8\% | 114.0 | 35.9 | 0.8 | 3.2 | 132.5 | 288.7 | 15.5 | 3.2 | 8.3 | 0.5 | 1.2 | 0.1 | 0.7 | 0.1 | 16.8 |
|  | 75 | 76 | 676 | 20.4\% | 102.6 | 31.7 | 0.8 | 2.9 | 157.2 | 335.4 | 15.9 | 2.7 | 7.7 | 0.5 | 1.1 | 0.1 | 0.7 | 0.1 | 16.5 |
|  | 76 | 77 | 1,133 | 22.0\% | 185.5 | 57.0 | 1.3 | 4.9 | 263.9 | 544.2 | 27.9 | 3.4 | 12.9 | 0.8 | 2.0 | 0.3 | 1.5 | 0.2 | 26.8 |
|  | 77 | 78 | 405 | 20.8\% | 62.8 | 18.8 | 0.6 | 2.3 | 93.7 | 196.5 | 10.0 | 2.0 | 5.2 | 0.4 | 0.9 | 0.1 | 0.6 | 0.1 | 11.4 |
| NEORB005 | 0 | 4 | 488 | 20.7\% | 73.9 | 23.0 | 0.8 | 3.5 | 114.5 | 233.4 | 11.0 | 1.3 | 6.4 | 0.6 | 1.5 | 0.2 | 1.0 | 0.2 | 16.6 |
|  | 4 | 8 | 935 | 20.9\% | 145.8 | 44.6 | 1.1 | 4.1 | 220.5 | 465.6 | 19.9 | 1.9 | 10.0 | 0.6 | 1.4 | 0.2 | 0.9 | 0.1 | 18.0 |
|  | 8 | 9 | 875 | 20.6\% | 133.0 | 41.8 | 1.0 | 4.2 | 205.2 | 437.3 | 17.5 | 1.8 | 9.1 | 0.7 | 1.8 | 0.2 | 1.2 | 0.2 | 19.6 |
|  | 9 | 10 | 781 | 20.9\% | 121.3 | 37.8 | 0.9 | 3.5 | 180.6 | 391.9 | 16.1 | 1.8 | 8.1 | 0.6 | 1.3 | 0.2 | 1.0 | 0.2 | 15.9 |
|  | 10 | 11 | 796 | 21.3\% | 126.0 | 39.0 | 0.9 | 3.2 | 184.1 | 398.0 | 17.5 | 2.1 | 8.5 | 0.5 | 1.1 | 0.1 | 0.8 | 0.1 | 13.6 |
|  | 11 | 12 | 745 | 21.5\% | 120.1 | 36.5 | 0.8 | 2.9 | 173.6 | 369.7 | 17.5 | 1.5 | 8.0 | 0.4 | 0.9 | 0.1 | 0.6 | 0.1 | 11.7 |
|  | 12 | 13 | 1,063 | 21.5\% | 170.3 | 52.8 | 1.2 | 4.2 | 255.7 | 518.4 | 25.4 | 3.0 | 11.6 | 0.6 | 1.4 | 0.1 | 1.0 | 0.1 | 16.8 |
|  | 13 | 14 | 615 | 22.2\% | 98.8 | 29.2 | 1.5 | 7.2 | 123.1 | 282.5 | 17.4 | 2.8 | 11.1 | 1.2 | 3.0 | 0.4 | 2.1 | 0.3 | 34.8 |
|  | 14 | 15 | 252 | 21.2\% | 39.4 | 12.2 | 0.4 | 1.5 | 57.6 | 121.9 | 6.3 | 0.9 | 3.2 | 0.3 | 0.6 | 0.1 | 0.5 | 0.1 | 7.4 |
|  | 15 | 16 | 163 | 20.4\% | 24.3 | 7.8 | 0.3 | 1.0 | 37.8 | 79.8 | 4.4 | 0.7 | 2.3 | 0.1 | 0.4 | 0.0 | 0.3 | 0.0 | 4.3 |
|  | 16 | 20 | 377 | 20.5\% | 57.6 | 17.9 | 0.4 | 1.4 | 90.5 | 189.2 | 8.2 | 1.3 | 3.9 | 0.2 | 0.5 | 0.1 | 0.3 | 0.1 | 5.7 |
|  | 20 | 24 | 604 | 20.1\% | 89.0 | 27.5 | 0.9 | 3.9 | 145.4 | 293.6 | 12.8 | 1.8 | 7.4 | 0.6 | 1.6 | 0.2 | 1.2 | 0.2 | 17.7 |
|  | 24 | 28 | 687 | 20.3\% | 103.3 | 32.9 | 0.8 | 2.6 | 164.2 | 341.5 | 15.2 | 2.3 | 7.4 | 0.4 | 1.1 | 0.1 | 0.8 | 0.1 | 14.6 |
|  | 28 | 29 | 555 | 20.7\% | 85.7 | 27.3 | 0.4 | 1.5 | 131.4 | 278.8 | 11.8 | 1.9 | 5.0 | 0.2 | 0.6 | 0.1 | 0.4 | 0.1 | 9.3 |
|  | 29 | 30 | 342 | 20.7\% | 52.1 | 16.9 | 0.3 | 1.4 | 73.7 | 175.7 | 7.1 | 1.6 | 3.3 | 0.2 | 0.6 | 0.1 | 0.5 | 0.1 | 8.3 |
|  | 30 | 31 | 2,223 | 21.9\% | 356.9 | 110.2 | 3.7 | 16.2 | 484.4 | 1,047.8 | 56.4 | 11.1 | 30.1 | 2.8 | 7.2 | 0.9 | 5.1 | 0.8 | 89.1 |
|  | 31 | 32 | 3,766 | 24.8\% | 702.2 | 187.3 | 8.0 | 36.0 | 828.0 | 1,609.2 | 111.0 | 21.8 | 70.7 | 6.1 | 16.6 | 2.1 | 12.9 | 1.8 | 152.4 |
|  | 32 | 33 | 415 | 19.9\% | 60.4 | 17.2 | 0.9 | 4.1 | 96.9 | 181.8 | 9.7 | 1.7 | 6.9 | 0.8 | 2.3 | 0.3 | 2.0 | 0.4 | 29.5 |
|  | 33 | 34 | 124 | 21.4\% | 19.4 | 5.6 | 0.3 | 1.3 | 24.9 | 54.9 | 4.5 | 0.6 | 2.9 | 0.2 | 0.8 | 0.1 | 0.9 | 0.2 | 7.7 |


| Hole ID | $\begin{gathered} \text { From } \\ (\mathrm{m}) \end{gathered}$ | To <br> (m) | $\begin{aligned} & \hline \text { TREO } \\ & \text { (ppm) } \end{aligned}$ | $\begin{gathered} \text { MREO: } \\ \text { TREO } \\ (\%) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline \mathrm{Nd}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \hline \mathrm{Pr}_{5} \mathrm{O}_{11} \\ & \text { (ppm) } \end{aligned}$ | $\begin{aligned} & \hline \mathrm{Tb}_{\mathrm{O}} \mathrm{O}_{7} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \mathrm{Dy}_{2} \mathrm{O}_{3} \\ (\mathrm{ppom}) \end{array} \end{aligned}$ | $\begin{aligned} & \mathrm{La}_{\mathrm{o}} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{CeO}_{2} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Sm}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Eu}_{3} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Cd}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \mathrm{Ho}_{2} \mathrm{O}_{3} \\ (\text { ppm } \end{array} \end{aligned}$ | $\begin{aligned} & \mathrm{Er}_{2} \mathrm{O}_{8} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \hline \mathrm{Tm}_{2} \mathrm{O}_{3} \\ & \text { (ppm) } \end{aligned}$ | $\begin{aligned} & \mathrm{Yb}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Lu}_{2} \mathrm{O}_{8} \\ & (\mathrm{ppmm}) \end{aligned}$ | $\begin{gathered} \mathrm{Y}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 34 | 35 | 94 | 21.4\% | 14.7 | 4.4 | 0.2 | 0.8 | 20.4 | 41.6 | 3.5 | 0.7 | 2.3 | 0.1 | 0.4 | 0.1 | 0.5 | 0.1 | 4.3 |
| NEORB006 | 0 | 4 | 320 | 21.8\% | 51.8 | 15.7 | 0.5 | 1.8 | 75.4 | 149.9 | 8.2 | 0.8 | 4.6 | 0.3 | 0.8 | 0.1 | 0.7 | 0.1 | 9.4 |
|  | 4 | 8 | 359 | 20.9\% | 56.1 | 17.8 | 0.3 | 0.9 | 90.8 | 175.7 | 8.3 | 0.7 | 3.9 | 0.1 | 0.3 | 0.0 | 0.1 | 0.0 | 3.6 |
|  | 8 | 12 | 438 | 21.4\% | 70.5 | 21.7 | 0.4 | 1.1 | 110.5 | 212.5 | 10.1 | 1.0 | 4.6 | 0.2 | 0.3 | 0.0 | 0.2 | 0.0 | 4.7 |
|  | 12 | 16 | 316 | 21.4\% | 50.6 | 15.8 | 0.3 | 0.8 | 78.3 | 154.8 | 7.3 | 0.7 | 3.4 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 3.2 |
|  | 16 | 20 | 206 | 19.9\% | 30.2 | 9.9 | 0.2 | 0.7 | 51.8 | 101.7 | 4.7 | 0.9 | 2.2 | 0.1 | 0.3 | 0.0 | 0.2 | 0.0 | 3.1 |
|  | 20 | 24 | 276 | 21.5\% | 44.2 | 14.0 | 0.3 | 0.8 | 66.3 | 136.4 | 6.8 | 1.2 | 3.0 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 2.9 |
|  | 24 | 28 | 435 | 20.3\% | 65.8 | 20.8 | 0.4 | 1.2 | 111.8 | 213.7 | 9.9 | 1.0 | 4.6 | 0.2 | 0.4 | 0.0 | 0.2 | 0.0 | 4.9 |
|  | 28 | 29 | 109 | 20.4\% | 16.6 | 5.2 | 0.1 | 0.4 | 27.9 | 52.6 | 2.6 | 0.5 | 1.3 | 0.1 | 0.1 | 0.0 | 0.1 | 0.0 | 1.8 |
|  | 29 | 30 | 371 | 21.6\% | 59.8 | 18.7 | 0.4 | 1.2 | 88.4 | 181.8 | 9.5 | 1.4 | 4.3 | 0.2 | 0.4 | 0.0 | 0.3 | 0.0 | 4.8 |
|  | 30 | 31 | 178 | 20.4\% | 26.9 | 8.6 | 0.2 | 0.6 | 45.4 | 86.5 | 4.0 | 0.8 | 1.9 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 2.3 |
|  | 31 | 32 | 351 | 21.5\% | 56.5 | 17.6 | 0.4 | 1.1 | 85.4 | 172.0 | 8.4 | 0.7 | 3.8 | 0.1 | 0.3 | 0.0 | 0.2 | 0.0 | 4.8 |
|  | 32 | 33 | 280 | 20.7\% | 43.2 | 13.7 | 0.3 | 0.8 | 70.0 | 137.6 | 6.7 | 0.8 | 3.1 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 3.2 |
|  | 33 | 34 | 1,181 | 17.2\% | 147.0 | 52.0 | 1.0 | 3.5 | 344.8 | 581.0 | 18.4 | 2.6 | 8.9 | 0.6 | 1.5 | 0.2 | 1.1 | 0.2 | 17.9 |
|  | 34 | 35 | 919 | 20.2\% | 136.5 | 44.3 | 1.0 | 3.4 | 238.1 | 444.7 | 18.6 | 2.3 | 9.0 | 0.6 | 1.5 | 0.2 | 1.1 | 0.1 | 17.9 |
|  | 35 | 36 | 756 | 19.8\% | 109.8 | 35.8 | 0.9 | 3.2 | 195.9 | 367.3 | 15.0 | 1.7 | 8.0 | 0.5 | 1.4 | 0.2 | 1.0 | 0.1 | 15.0 |
|  | 36 | 37 | 792 | 19.8\% | 115.6 | 37.0 | 0.9 | 3.4 | 207.6 | 382.0 | 15.7 | 1.9 | 8.6 | 0.6 | 1.5 | 0.2 | 1.1 | 0.2 | 15.9 |
|  | 37 | 38 | 879 | 22.1\% | 144.6 | 45.1 | 1.0 | 3.6 | 209.9 | 422.6 | 19.5 | 2.3 | 9.4 | 0.6 | 1.5 | 0.2 | 1.1 | 0.2 | 17.9 |
|  | 38 | 39 | 877 | 21.5\% | 141.1 | 42.9 | 1.1 | 3.9 | 211.1 | 422.6 | 19.7 | 2.3 | 10.0 | 0.7 | 1.7 | 0.2 | 1.3 | 0.2 | 18.7 |
|  | 39 | 40 | 649 | 20.1\% | 96.3 | 30.7 | 0.8 | 2.8 | 168.9 | 310.8 | 13.9 | 1.9 | 7.3 | 0.5 | 1.1 | 0.1 | 0.7 | 0.1 | 13.5 |
|  | 40 | 41 | 709 | 21.5\% | 112.4 | 35.3 | 1.0 | 3.9 | 170.1 | 335.4 | 16.1 | 2.2 | 8.7 | 0.7 | 1.8 | 0.2 | 1.5 | 0.2 | 19.6 |
|  | 41 | 42 | 931 | 21.1\% | 144.6 | 46.4 | 1.2 | 4.2 | 226.4 | 449.6 | 19.9 | 3.3 | 10.1 | 0.7 | 1.7 | 0.2 | 1.3 | 0.2 | 21.1 |
|  | 42 | 43 | 1,185 | 22.8\% | 200.6 | 62.0 | 1.6 | 5.5 | 258.0 | 577.3 | 29.6 | 5.5 | 13.5 | 1.0 | 2.4 | 0.3 | 1.9 | 0.3 | 25.5 |
|  | 43 | 44 | 1,220 | 22.3\% | 203.0 | 62.0 | 1.6 | 6.0 | 267.4 | 595.8 | 28.2 | 5.2 | 14.1 | 1.0 | 2.8 | 0.4 | 2.5 | 0.4 | 29.3 |
|  | 44 | 45 | 1,455 | 21.1\% | 227.4 | 71.5 | 1.9 | 6.7 | 348.3 | 707.6 | 31.2 | 4.5 | 16.3 | 1.1 | 3.2 | 0.4 | 2.7 | 0.4 | 31.4 |
|  | 45 | 46 | 1,899 | 19.5\% | 269.4 | 89.6 | 2.5 | 8.9 | 491.4 | 921.3 | 41.7 | 9.1 | 19.9 | 1.5 | 3.9 | 0.5 | 3.3 | 0.5 | 35.4 |
|  | 46 | 47 | 1,016 | 25.5\% | 191.3 | 56.2 | 2.3 | 8.7 | 172.4 | 472.9 | 35.9 | 9.4 | 19.1 | 1.4 | 3.8 | 0.5 | 3.0 | 0.4 | 38.2 |
|  | 47 | 48 | 916 | 21.0\% | 141.1 | 42.4 | 1.9 | 7.0 | 217.0 | 420.1 | 26.2 | 7.2 | 15.7 | 1.2 | 3.1 | 0.4 | 2.4 | 0.3 | 30.2 |
|  | 48 | 49 | 1,023 | 18.6\% | 137.6 | 44.1 | 1.7 | 6.9 | 282.6 | 475.4 | 23.3 | 6.7 | 14.3 | 0.9 | 2.4 | 0.3 | 1.7 | 0.2 | 24.6 |
|  | 49 | 50 | 1,014 | 20.3\% | 149.3 | 44.8 | 2.4 | 9.5 | 241.6 | 450.8 | 26.6 | 8.6 | 19.8 | 1.7 | 4.5 | 0.6 | 3.4 | 0.5 | 50.2 |
|  | 50 | 51 | 909 | 23.4\% | 156.3 | 46.0 | 2.2 | 8.0 | 180.6 | 421.3 | 29.1 | 8.5 | 18.2 | 1.3 | 3.3 | 0.5 | 2.7 | 0.4 | 30.9 |
|  | 51 | 52 | 455 | 24.2\% | 81.5 | 23.7 | 1.1 | 3.9 | 85.1 | 212.5 | 15.5 | 4.5 | 9.4 | 0.6 | 1.5 | 0.2 | 1.3 | 0.2 | 14.3 |
|  | 52 | 53 | 693 | 24.8\% | 128.3 | 36.7 | 1.6 | 5.3 | 129.0 | 324.3 | 23.7 | 6.5 | 13.7 | 0.8 | 1.9 | 0.3 | 1.5 | 0.2 | 19.3 |
|  | 53 | 54 | 394 | 23.0\% | 67.4 | 19.6 | 0.8 | 2.8 | 84.8 | 181.8 | 11.8 | 3.4 | 7.2 | 0.4 | 1.1 | 0.1 | 0.8 | 0.1 | 11.8 |
|  | 54 | 55 | 534 | 23.2\% | 92.1 | 26.2 | 1.3 | 4.4 | 112.7 | 242.0 | 17.2 | 4.4 | 11.2 | 0.7 | 1.8 | 0.2 | 1.5 | 0.2 | 18.0 |
|  | 55 | 56 | 610 | 23.3\% | 105.4 | 29.1 | 1.4 | 5.9 | 131.4 | 270.2 | 18.6 | 4.9 | 12.8 | 0.9 | 2.0 | 0.3 | 1.5 | 0.2 | 25.1 |
|  | 56 | 60 | 381 | 23.7\% | 66.8 | 18.1 | 1.0 | 4.3 | 81.4 | 163.4 | 12.1 | 3.3 | 9.1 | 0.6 | 1.6 | 0.2 | 1.5 | 0.2 | 17.5 |
|  | 60 | 61 | 250 | 23.7\% | 43.9 | 11.9 | 0.7 | 2.7 | 51.3 | 106.5 | 9.5 | 1.5 | 7.0 | 0.4 | 1.1 | 0.2 | 1.1 | 0.2 | 11.8 |
|  | 61 | 62 | 319 | 25.0\% | 59.3 | 15.2 | 1.0 | 4.3 | 65.2 | 129.0 | 11.7 | 2.9 | 9.2 | 0.6 | 1.7 | 0.2 | 1.4 | 0.2 | 17.7 |
|  | 62 | 63 | 721 | 24.9\% | 133.0 | 34.9 | 2.1 | 9.3 | 145.4 | 294.8 | 24.9 | 6.0 | 18.4 | 1.4 | 3.5 | 0.5 | 3.0 | 0.4 | 43.2 |
|  | 63 | 64 | 605 | 24.6\% | 109.6 | 28.9 | 1.7 | 8.4 | 122.0 | 243.2 | 20.2 | 5.0 | 15.1 | 1.4 | 3.4 | 0.4 | 2.7 | 0.4 | 42.4 |
|  | 64 | 65 | 369 | 21.4\% | 57.7 | 17.2 | 0.7 | 3.4 | 79.2 | 169.5 | 9.3 | 1.5 | 5.8 | 0.6 | 1.6 | 0.2 | 1.3 | 0.2 | 20.8 |
| NEORB007 | 0 | 4 | 354 | 21.6\% | 56.8 | 17.8 | 0.4 | 1.4 | 84.4 | 173.2 | 7.9 | 1.1 | 3.7 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 6.0 |
|  | 4 | 5 | 1,413 | 21.3\% | 227.4 | 69.6 | 1.0 | 3.3 | 351.8 | 700.2 | 29.7 | 2.4 | 12.3 | 0.4 | 1.1 | 0.1 | 0.8 | 0.1 | 12.6 |
|  | 5 | 6 | 508 | 21.9\% | 83.7 | 25.6 | 0.4 | 1.4 | 122.0 | 250.6 | 11.3 | 1.2 | 4.7 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 5.6 |
|  | 6 | 7 | 612 | 21.4\% | 98.6 | 30.4 | 0.5 | 1.6 | 147.8 | 303.4 | 13.2 | 1.8 | 5.2 | 0.2 | 0.6 | 0.1 | 0.5 | 0.1 | 7.7 |
|  | 7 | 8 | 367 | 21.0\% | 57.7 | 18.0 | 0.3 | 1.1 | 91.2 | 180.6 | 8.2 | 1.1 | 3.7 | 0.1 | 0.3 | 0.0 | 0.2 | 0.0 | 4.4 |
|  | 8 | 12 | 399 | 20.8\% | 61.7 | 19.7 | 0.4 | 1.3 | 99.2 | 196.5 | 8.2 | 1.4 | 3.7 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 6.1 |
|  | 12 | 16 | 147 | 19.3\% | 20.9 | 6.7 | 0.2 | 0.6 | 39.2 | 70.8 | 3.0 | 1.4 | 1.4 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 2.3 |
|  | 16 | 20 | 322 | 20.9\% | 48.6 | 15.1 | 0.6 | 3.2 | 74.8 | 148.6 | 7.5 | 1.1 | 4.5 | 0.5 | 1.5 | 0.2 | 1.4 | 0.2 | 14.5 |
|  | 20 | 21 | 279 | 23.4\% | 47.2 | 13.5 | 0.8 | 3.7 | 53.9 | 120.1 | 8.1 | 1.5 | 5.5 | 0.7 | 2.0 | 0.3 | 2.0 | 0.3 | 19.3 |
|  | 21 | 22 | 299 | 24.3\% | 52.5 | 14.9 | 0.9 | 4.4 | 56.8 | 129.0 | 9.1 | 1.8 | 6.4 | 0.7 | 2.0 | 0.3 | 1.7 | 0.3 | 18.5 |
|  | 22 | 23 | 281 | 24.0\% | 49.2 | 13.8 | 0.8 | 3.8 | 54.2 | 124.1 | 8.7 | 1.6 | 6.1 | 0.6 | 1.5 | 0.2 | 1.4 | 0.2 | 14.9 |
|  | $\begin{array}{r}23 \\ 24 \\ \hline\end{array}$ | 24 | 255 | 23.9\% | 44.6 | 12.7 | 0.7 | 3.0 | 52.3 | 112.4 | 8.0 | 1.0 | 5.6 | 0.4 | 1.1 | 0.1 | 1.1 | 0.2 | 11.9 |
|  | 24 | 28 | 252 | 23.9\% | 44.0 | 12.6 | 0.6 | 2.9 | 52.2 | 111.2 | 7.6 | 1.0 | 5.5 | 0.4 | 1.1 | 0.2 | 1.2 | 0.2 | 11.2 |
|  | 28 | 32 | 253 | 23.8\% | 44.1 | 12.8 | 0.7 | 2.9 | 51.8 | 112.3 | 7.6 | 1.1 | 5.3 | 0.5 | 1.1 | 0.2 | 1.1 | 0.2 | 11.8 |


| Hole ID | $\begin{aligned} & \text { From } \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \hline \text { To } \\ & \text { (m) } \end{aligned}$ | TREO (ppm) | $\begin{gathered} \hline \text { MREO: } \\ \text { TREO } \end{gathered}$ (\%) | $\mathrm{Nd}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{Pr}_{6} \mathrm{O}_{11} \\ & \text { (ppm) } \end{aligned}$ | $\mathrm{Tb}_{4} \mathrm{O}_{7}$ (ppm) | $\begin{aligned} & \hline \begin{array}{l} \mathrm{Dy}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{array} \end{aligned}$ | $\begin{aligned} & \hline \mathrm{La}_{2} \mathrm{O}_{8} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{CeO}_{2}$ (ppm) | $\mathrm{Sm}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & E \mathrm{U}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Cd}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Ho}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Er}_{2} \mathrm{O}_{8} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{Tm}_{2} \mathrm{O}_{3}$ (ppm) | $\mathrm{Yb}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \hline \mathrm{L}_{2} \mathrm{O}_{8} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \mathrm{Y}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{array} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 32 | 36 | 367 | 23.0\% | 61.8 | 18.1 | 0.7 | 3.5 | 76.9 | 170.7 | 9.9 | 1.2 | 6.2 | 0.5 | 1.5 | 0.2 | 1.3 | 0.2 | 13.7 |
|  | 36 | 40 | 274 | 23.3\% | 46.7 | 13.5 | 0.7 | 3.0 | 59.8 | 122.8 | 8.0 | 1.4 | 6.0 | 0.4 | 0.9 | 0.1 | 0.7 | 0.1 | 9.9 |
|  | 40 | 41 | 1,049 | 22.0\% | 165.6 | 47.1 | 2.8 | 15.1 | 224.0 | 442.2 | 26.6 | 5.1 | 21.7 | 2.7 | 7.1 | 0.9 | 6.0 | 0.9 | 81.0 |
|  | 41 | 42 | 294 | 23.1\% | 49.9 | 14.1 | 0.7 | 3.1 | 62.9 | 132.7 | 8.7 | 1.6 | 5.9 | 0.4 | 1.0 | 0.1 | 0.8 | 0.1 | 11.6 |
|  | 42 | 43 | 964 | 21.1\% | 142.3 | 39.9 | 3.1 | 17.8 | 199.4 | 378.3 | 24.0 | 4.7 | 21.7 | 3.3 | 9.2 | 1.2 | 7.6 | 1.2 | 110.4 |
|  | 43 | 44 | 282 | 23.0\% | 47.6 | 13.5 | 0.7 | 3.0 | 60.0 | 126.5 | 8.1 | 1.5 | 5.5 | 0.4 | 1.0 | 0.1 | 0.8 | 0.1 | 12.5 |
|  | 44 | 48 | 304 | 22.5\% | 49.7 | 14.5 | 0.7 | 3.4 | 66.3 | 137.6 | 8.3 | 1.3 | 5.7 | 0.5 | 1.3 | 0.2 | 1.2 | 0.2 | 13.5 |
|  | 48 | 49 | 873 | 24.4\% | 156.3 | 44.1 | 2.2 | 10.2 | 170.1 | 386.9 | 26.4 | 5.2 | 17.1 | 1.7 | 4.3 | 0.5 | 3.7 | 0.5 | 44.2 |
|  | 49 | 50 | 635 | 24.1\% | 112.0 | 32.4 | 1.4 | 7.4 | 125.5 | 285.0 | 18.4 | 3.4 | 11.5 | 1.2 | 3.1 | 0.4 | 3.0 | 0.4 | 29.7 |
|  | 50 | 51 | 531 | 22.8\% | 87.6 | 26.3 | 1.1 | 5.8 | 105.8 | 245.7 | 14.3 | 2.4 | 8.7 | 1.0 | 2.6 | 0.4 | 2.3 | 0.4 | 26.4 |
|  | 51 | 52 | 510 | 24.2\% | 90.0 | 25.6 | 1.3 | 6.7 | 98.0 | 224.8 | 15.0 | 2.9 | 9.8 | 1.1 | 2.7 | 0.4 | 2.3 | 0.4 | 29.3 |
|  | 52 | 56 | 504 | 24.2\% | 88.4 | 25.5 | 1.3 | 6.8 | 95.3 | 222.3 | 15.0 | 3.1 | 9.6 | 1.1 | 2.9 | 0.4 | 2.5 | 0.4 | 28.8 |
|  | 56 | 57 | 1,002 | 23.4\% | 170.3 | 53.2 | 1.9 | 9.3 | 197.0 | 475.4 | 26.3 | 4.5 | 14.8 | 1.5 | 4.0 | 0.5 | 3.2 | 0.4 | 39.5 |
|  | 57 | 58 | 977 | 24.6\% | 176.1 | 49.5 | 2.6 | 12.2 | 192.3 | 427.5 | 30.6 | 7.0 | 19.8 | 2.0 | 4.8 | 0.6 | 3.9 | 0.5 | 47.0 |
|  | 58 | 59 | 540 | 24.1\% | 94.7 | 26.6 | 1.5 | 7.3 | 110.8 | 233.4 | 17.5 | 3.4 | 11.5 | 1.2 | 2.9 | 0.4 | 2.6 | 0.4 | 25.7 |
|  | 59 | 60 | 308 | 23.0\% | 50.9 | 14.3 | 0.9 | 4.7 | 61.7 | 126.5 | 9.7 | 1.9 | 6.8 | 0.8 | 2.4 | 0.3 | 2.1 | 0.3 | 24.3 |
|  | 60 | 61 | 838 | 21.5\% | 127.1 | 36.7 | 2.5 | 13.9 | 171.2 | 331.7 | 23.5 | 4.4 | 19.6 | 2.7 | 7.4 | 1.0 | 6.0 | 0.9 | 89.9 |
|  | 61 | 62 | 723 | 23.2\% | 120.1 | 34.2 | 2.2 | 10.9 | 143.1 | 302.2 | 22.8 | 4.0 | 15.9 | 1.9 | 5.3 | 0.7 | 4.7 | 0.7 | 54.2 |
|  | 62 | 63 | 497 | 22.9\% | 80.9 | 23.1 | 1.6 | 8.1 | 96.9 | 210.1 | 15.4 | 3.2 | 11.6 | 1.4 | 3.9 | 0.5 | 3.5 | 0.5 | 36.4 |
| NEORB008 | 0 | 4 | 335 | 20.9\% | 49.7 | 15.0 | 0.9 | 4.5 | 73.9 | 147.4 | 8.8 | 1.5 | 6.2 | 0.8 | 2.2 | 0.3 | 1.9 | 0.3 | 22.1 |
|  | 4 | 8 | 202 | 22.5\% | 32.2 | 9.4 | 0.6 | 3.3 | 40.3 | 86.4 | 6.0 | 1.0 | 4.5 | 0.6 | 1.7 | 0.3 | 1.8 | 0.3 | 13.7 |
|  | 8 | 12 | 452 | 21.8\% | 70.1 | 21.3 | 1.2 | 5.8 | 94.8 | 202.7 | 13.0 | 2.4 | 8.3 | 1.0 | 2.6 | 0.3 | 2.0 | 0.3 | 25.8 |
|  | 12 | 13 | 1,263 | 19.8\% | 178.5 | 63.6 | 1.5 | 6.5 | 315.5 | 625.3 | 24.4 | 4.4 | 11.9 | 1.0 | 2.4 | 0.3 | 1.5 | 0.2 | 26.2 |
|  | 13 | 14 | 879 | 21.1\% | 133.0 | 42.3 | 1.7 | 8.6 | 207.6 | 402.9 | 19.5 | 4.4 | 13.6 | 1.4 | 3.3 | 0.3 | 1.9 | 0.3 | 38.1 |
|  | 14 | 15 | 701 | 21.2\% | 104.6 | 30.0 | 2.2 | 11.7 | 150.1 | 285.0 | 18.8 | 5.1 | 15.6 | 2.1 | 5.8 | 0.8 | 4.7 | 0.6 | 64.0 |
|  | 15 | 16 | 1,104 | 21.7\% | 172.6 | 52.3 | 2.3 | 11.8 | 252.2 | 488.9 | 27.8 | 6.2 | 18.4 | 2.0 | 5.3 | 0.7 | 4.3 | 0.6 | 58.2 |
|  | 16 | 20 | 910 | 21.2\% | 141.1 | 43.6 | 1.5 | 7.0 | 206.4 | 428.7 | 21.9 | 4.9 | 12.7 | 1.1 | 3.0 | 0.4 | 2.2 | 0.3 | 34.7 |
|  | 20 | 24 | 550 | 22.3\% | 90.7 | 28.0 | 0.8 | 3.1 | 124.3 | 265.3 | 13.5 | 1.5 | 6.8 | 0.5 | 1.1 | 0.1 | 0.8 | 0.1 | 13.8 |
|  | 24 | 28 | 540 | 23.1\% | 90.7 | 27.2 | 1.3 | 5.3 | 112.5 | 245.7 | 16.5 | 2.8 | 10.0 | 0.8 | 1.9 | 0.2 | 1.3 | 0.2 | 23.6 |
|  | 28 | 29 | 399 | 24.5\% | 71.9 | 20.1 | 1.1 | 4.6 | 80.9 | 176.9 | 12.6 | 2.3 | 9.0 | 0.7 | 1.4 | 0.1 | 1.0 | 0.1 | 15.9 |
|  | 29 | 30 | 395 | 24.2\% | 70.5 | 19.9 | 1.1 | 4.4 | 81.2 | 176.9 | 12.9 | 2.2 | 8.8 | 0.6 | 1.3 | 0.2 | 0.8 | 0.1 | 14.7 |
|  | 30 | 31 | 810 | 23.7\% | 141.1 | 40.4 | 2.1 | 8.5 | 168.9 | 364.8 | 26.4 | 4.6 | 17.4 | 1.1 | 2.4 | 0.2 | 1.4 | 0.2 | 29.8 |
|  | 31 | 32 | 393 | 24.1\% | 69.6 | 19.6 | 1.1 | 4.4 | 82.2 | 174.4 | 12.9 | 2.4 | 9.3 | 0.6 | 1.3 | 0.1 | 0.7 | 0.1 | 14.5 |
|  | 32 | 36 | 228 | 22.1\% | 36.3 | 10.7 | 0.6 | 2.6 | 49.0 | 101.6 | 6.5 | 1.6 | 4.7 | 0.4 | 1.0 | 0.1 | 0.9 | 0.1 | 11.4 |
|  | 36 | 37 | 480 | 23.8\% | 82.9 | 23.6 | 1.5 | 6.4 | 94.5 | 208.8 | 16.0 | 3.3 | 11.8 | 0.9 | 2.2 | 0.3 | 1.5 | 0.2 | 25.8 |
|  | 37 | 38 | 762 | 23.5\% | 131.8 | 37.9 | 1.9 | 7.7 | 161.8 | 341.5 | 24.7 | 4.5 | 16.1 | 1.0 | 2.5 | 0.3 | 3.0 | 0.3 | 27.3 |
|  | 38 | 39 | 514 | 24.1\% | 90.0 | 25.6 | 1.6 | 6.7 | 104.4 | 222.3 | 16.9 | 3.5 | 12.0 | 1.0 | 2.3 | 0.3 | 1.7 | 0.2 | 25.5 |
|  | 39 | 40 | 564 | 23.3\% | 96.1 | 28.2 | 1.4 | 6.0 | 118.5 | 255.5 | 16.6 | 3.4 | 10.9 | 0.9 | 2.0 | 0.2 | 1.5 | 0.2 | 23.1 |
|  | 40 | 41 | 603 | 22.1\% | 95.1 | 29.0 | 1.6 | 7.5 | 130.2 | 271.5 | 16.6 | 4.2 | 12.0 | 1.1 | 2.8 | 0.3 | 2.3 | 0.4 | 28.8 |
|  | 41 | 42 | 896 | 25.9\% | 165.6 | 43.1 | 4.1 | 19.5 | 152.5 | 350.1 | 36.1 | 12.4 | 27.5 | 3.0 | 7.7 | 1.0 | 7.2 | 1.0 | 65.7 |
|  | 42 | 43 | 1,157 | 28.1\% | 230.9 | 57.6 | 6.2 | 30.6 | 177.1 | 423.8 | 52.9 | 19.1 | 41.7 | 4.8 | 11.7 | 1.6 | 10.8 | 1.4 | 86.6 |
|  | 43 | 44 | 975 | 27.6\% | 193.6 | 47.5 | 4.8 | 22.8 | 157.2 | 369.7 | 42.7 | 14.6 | 33.0 | 3.5 | 8.7 | 1.1 | 7.9 | 1.0 | 67.1 |
|  | 44 | 45 | 687 | 25.6\% | 127.1 | 33.8 | 2.6 | 12.5 | 123.1 | 282.5 | 25.7 | 7.5 | 19.6 | 1.8 | 4.6 | 0.6 | 4.2 | 0.5 | 40.9 |
|  | 45 | 46 | 910 | 27.5\% | 178.5 | 45.9 | 4.3 | 21.2 | 146.6 | 350.1 | 38.5 | 12.5 | 29.9 | 3.3 | 8.2 | 1.1 | 7.1 | 1.0 | 62.2 |
|  | 46 | 47 | 516 | 27.3\% | 101.0 | 25.1 | 2.5 | 12.1 | 83.4 | 196.5 | 22.0 | 7.1 | 17.2 | 1.9 | 4.8 | 0.6 | 4.3 | 0.5 | 36.7 |
|  | 47 | 48 | 504 | 27.4\% | 97.3 | 24.0 | 2.8 | 13.9 | 75.3 | 183.0 | 22.5 | 8.4 | 19.5 | 2.1 | 5.5 | 0.8 | 5.1 | 0.7 | 43.2 |
|  | 48 | 49 | 641 | 27.6\% | 124.8 | 30.4 | 3.8 | 17.8 | 92.7 | 229.7 | 29.0 | 11.1 | 25.8 | 2.8 | 7.0 | 1.0 | 6.6 | 0.8 | 57.1 |
|  | 49 | 50 | 751 | 26.6\% | 140.0 | 34.9 | 4.2 | 20.3 | 116.0 | 271.5 | 31.4 | 11.7 | 29.5 | 3.3 | 8.2 | 1.2 | 7.3 | 1.0 | 70.6 |
|  | 50 | 51 | 654 | 25.3\% | 116.1 | 29.8 | 3.4 | 16.4 | 111.4 | 244.5 | 25.5 | 8.7 | 24.4 | 2.7 | 6.7 | 1.0 | 5.9 | 0.8 | 56.8 |
|  | 51 | 52 | 493 | 25.6\% | 85.8 | 21.0 | 3.1 | 16.4 | 74.2 | 162.1 | 19.4 | 7.6 | 21.0 | 2.8 | 7.5 | 1.1 | 6.9 | 0.9 | 63.2 |
|  | 52 | 53 | 529 | 26.2\% | 95.3 | 23.0 | 3.2 | 17.1 | 74.5 | 175.7 | 21.5 | 8.6 | 23.4 | 2.9 | 8.0 | 1.1 | 6.8 | 0.9 | 67.1 |
|  | 53 | 54 | 481 | 26.8\% | 90.9 | 23.1 | 2.6 | 12.4 | 72.0 | 173.2 | 20.9 | 7.9 | 18.9 | 2.1 | 5.6 | 0.8 | 4.9 | 0.7 | 44.6 |
|  | 54 | 55 | 173 | 20.9\% | 25.4 | 7.8 | 0.5 | 2.3 | 38.0 | 74.6 | 4.9 | 0.9 | 3.7 | 0.4 | 1.1 | 0.2 | 1.2 | 0.2 | 11.3 |
|  | 55 | 56 | 200 | 20.7\% | 28.9 | 9.0 | 0.6 | 3.0 | 42.7 | 84.3 | 5.6 | 1.0 | 4.3 | 0.6 | 1.9 | 0.3 | 2.2 | 0.3 | 15.7 |
|  | 56 | 57 | 320 | 21.3\% | 47.9 | 14.3 | 0.9 | 5.1 | 65.1 | 132.7 | 9.4 | 1.6 | 7.0 | 1.0 | 3.1 | 0.5 | 3.4 | 0.5 | 27.4 |
|  | 57 | 58 | 233 | 20.6\% | 33.7 | 10.4 | 0.7 | 3.3 | 51.7 | 99.3 | 6.9 | 1.6 | 5.4 | 0.6 | 1.7 | 0.3 | 1.7 | 0.3 | 15.7 |
|  | 58 | 59 | 254 | 20.6\% | 36.7 | 11.3 | 0.8 | 3.5 | 54.2 | 107.9 | 7.7 | 1.6 | 5.5 | 0.7 | 1.8 | 0.3 | 1.8 | 0.3 | 19.8 |

## VOLTAIC

| Hole ID | $\begin{aligned} & \text { From } \\ & (\mathrm{m}) \end{aligned}$ | To <br> (m) | $\begin{aligned} & \text { TREO } \\ & \text { (ppm) } \end{aligned}$ | $\begin{gathered} \text { MREO: } \\ \text { TREO } \\ (\%) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline \mathrm{Nd}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Pr}_{\mathrm{Pr} \mathrm{O}_{11}}^{(\mathrm{ppom})} \end{aligned}$ | $\begin{aligned} & \mathrm{Tb}_{4} \mathrm{O}_{7} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \mathrm{Dy}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{array} \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \mathrm{La}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{array} \end{aligned}$ | $\begin{aligned} & \mathrm{CeO}_{2} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Sm}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Eu}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Cd}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppmm}) \end{aligned}$ | $\mathrm{Ho}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{Er}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{Tm}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{Yb}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Lu}_{2} \mathrm{O}_{8} \\ & (\mathrm{ppmm}) \end{aligned}$ | $\begin{gathered} \mathrm{r}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 59 | 60 | 967 | 19.4\% | 134.1 | 44.3 | 1.6 | 7.9 | 245.1 | 445.9 | 19.8 | 3.6 | 12.8 | 1.4 | 3.9 | 0.6 | 3.9 | 0.6 | 41.1 |
|  | 60 | 61 | 308 | 20.7\% | 45.3 | 13.5 | 0.9 | 4.2 | 70.4 | 130.2 | 9.1 | 2.0 | 6.7 | 0.7 | 2.4 | 0.3 | 2.0 | 0.4 | 19.8 |
|  | 61 | 62 | 476 | 22.5\% | 76.0 | 22.1 | 1.6 | 7.5 | 98.9 | 196.5 | 15.3 | 4.1 | 11.9 | 1.2 | 3.4 | 0.5 | 3.1 | 0.5 | 33.3 |
|  | 62 | 63 | 374 | 22.4\% | 60.3 | 17.3 | 1.2 | 4.9 | 79.9 | 158.5 | 12.3 | 2.8 | 9.0 | 0.8 | 2.1 | 0.3 | 1.9 | 0.3 | 22.7 |
|  | 63 | 64 | 448 | 22.1\% | 71.2 | 21.3 | 1.3 | 5.5 | 100.6 | 192.9 | 13.9 | 3.3 | 10.4 | 0.8 | 2.0 | 0.3 | 1.6 | 0.3 | 23.0 |
|  | 64 | 65 | 379 | 22.3\% | 60.8 | 17.9 | 1.2 | 4.6 | 81.9 | 165.8 | 12.2 | 2.4 | 8.8 | 0.7 | 2.0 | 0.2 | 1.3 | 0.2 | 18.9 |
|  | 65 | 66 | 276 | 22.4\% | 44.6 | 12.9 | 0.9 | 3.6 | 57.9 | 120.1 | 8.8 | 1.7 | 6.8 | 0.5 | 1.3 | 0.2 | 1.2 | 0.2 | 15.6 |
|  | 66 | 67 | 479 | 20.8\% | 70.8 | 21.9 | 1.3 | 5.7 | 108.0 | 210.1 | 13.9 | 2.6 | 10.3 | 0.9 | 2.6 | 0.4 | 2.3 | 0.4 | 28.1 |
|  | 67 | 68 | 562 | 21.3\% | 84.8 | 25.0 | 1.8 | 8.4 | 122.0 | 235.9 | 16.1 | 3.3 | 12.2 | 1.5 | 4.1 | 0.6 | 3.7 | 0.5 | 42.3 |
|  | 68 | 69 | 466 | 21.5\% | 70.8 | 20.4 | 1.4 | 7.5 | 93.0 | 189.2 | 13.6 | 2.8 | 10.0 | 1.5 | 4.4 | 0.7 | 4.4 | 0.7 | 45.6 |
|  | 69 | 70 | 425 | 22.1\% | 66.7 | 19.0 | 1.3 | 6.9 | 85.7 | 174.4 | 11.8 | 2.8 | 9.4 | 1.3 | 3.7 | 0.5 | 3.5 | 0.5 | 37.3 |
|  | 70 | 71 | 363 | 21.3\% | 53.8 | 15.5 | 1.3 | 6.9 | 67.1 | 140.0 | 10.5 | 2.3 | 9.1 | 1.5 | 4.6 | 0.7 | 4.6 | 0.7 | 44.6 |
|  | 71 | 72 | 558 | 21.9\% | 87.2 | 26.1 | 1.5 | 7.1 | 119.6 | 242.0 | 15.0 | 3.1 | 11.3 | 1.3 | 3.4 | 0.5 | 3.1 | 0.4 | 36.3 |
|  | 72 | 73 | 433 | 21.7\% | 67.7 | 20.5 | 1.1 | 4.8 | 92.3 | 190.4 | 11.7 | 1.9 | 8.1 | 0.9 | 2.5 | 0.3 | 2.1 | 0.3 | 28.3 |
|  | 73 | 74 | 221 | 21.3\% | 33.1 | 10.1 | 0.7 | 3.0 | 49.0 | 93.6 | 6.5 | 1.1 | 4.9 | 0.5 | 1.3 | 0.2 | 1.3 | 0.2 | 15.1 |
|  | 74 | 75 | 261 | 21.8\% | 40.4 | 11.8 | 0.8 | 3.9 | 54.1 | 108.0 | 7.7 | 1.2 | 5.9 | 0.7 | 2.4 | 0.3 | 2.3 | 0.4 | 21.3 |
| NEORB009 | 0 | 4 | 358 | 20.7\% | 54.1 | 17.0 | 0.5 | 2.4 | 87.0 | 167.1 | 8.7 | 1.6 | 4.8 | 0.4 | 1.1 | 0.2 | 1.0 | 0.2 | 12.2 |
|  | 4 | 8 | 191 | 21.1\% | 29.3 | 8.9 | 0.4 | 1.7 | 43.0 | 86.1 | 5.5 | 1.2 | 3.4 | 0.3 | 0.9 | 0.1 | 0.7 | 0.1 | 9.1 |
|  | 8 | 9 | 309 | 22.2\% | 47.5 | 13.2 | 1.3 | 6.8 | 54.3 | 118.0 | 10.3 | 1.8 | 8.9 | 1.4 | 4.2 | 0.6 | 3.8 | 0.6 | 36.8 |
|  | 9 | 10 | 334 | 21.1\% | 50.2 | 15.3 | 0.7 | 4.2 | 73.1 | 147.4 | 8.6 | 1.3 | 6.3 | 0.7 | 2.2 | 0.3 | 2.2 | 0.3 | 21.3 |
|  | 10 | 11 | 183 | 21.3\% | 27.4 | 8.1 | 0.6 | 3.0 | 36.6 | 75.4 | 5.3 | 0.8 | 4.2 | 0.6 | 1.7 | 0.3 | 1.7 | 0.3 | 17.3 |
|  | 11 | 12 | 67 | 19.9\% | 8.7 | 2.7 | 0.3 | 1.6 | 12.2 | 25.6 | 2.1 | 0.6 | 1.8 | 0.3 | 0.9 | 0.1 | 0.7 | 0.1 | 9.3 |
|  | 12 | 13 | 276 | 21.0\% | 41.6 | 12.8 | 0.6 | 3.0 | 60.3 | 125.3 | 7.3 | 1.4 | 4.9 | 0.5 | 1.3 | 0.2 | 1.0 | 0.2 | 15.9 |
|  | 13 | 14 | 151 | 20.6\% | 22.3 | 6.8 | 0.3 | 1.7 | 32.8 | 68.5 | 4.1 | 0.8 | 2.6 | 0.3 | 0.7 | 0.1 | 0.6 | 0.1 | 8.9 |
|  | 14 | 15 | 139 | 21.8\% | 21.0 | 6.1 | 0.5 | 2.8 | 27.0 | 55.9 | 4.2 | 0.8 | 3.4 | 0.5 | 1.3 | 0.2 | 1.2 | 0.2 | 13.8 |
| NEORB010 | 0 | 4 | 207 | 20.8\% | 31.7 | 9.9 | 0.3 | 1.3 | 48.4 | 99.5 | 4.9 | 1.2 | 2.7 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 6.3 |
|  | 4 | 5 | 256 | 21.0\% | 40.1 | 12.2 | 0.3 | 1.1 | 62.4 | 124.1 | 5.9 | 1.3 | 3.0 | 0.1 | 0.3 | 0.0 | 0.3 | 0.0 | 5.0 |
|  | 5 | 6 | 1,240 | 21.1\% | 194.8 | 62.3 | 1.1 | 3.6 | 304.9 | 613.0 | 28.6 | 2.2 | 13.5 | 0.5 | 0.9 | 0.1 | 0.5 | 0.1 | 14.1 |
|  | 6 | 7 | 151 | 21.1\% | 23.6 | 7.2 | 0.2 | 0.9 | 35.4 | 71.7 | 3.7 | 1.2 | 1.9 | 0.1 | 0.3 | 0.0 | 0.3 | 0.0 | 4.2 |
|  | 7 | 8 | 574 | 21.1\% | 90.6 | 28.5 | 0.6 | 1.7 | 141.9 | 281.3 | 13.6 | 2.0 | 6.5 | 0.2 | 0.5 | 0.0 | 0.3 | 0.0 | 6.8 |
|  | 8 | 9 | 292 | 20.7\% | 44.9 | 14.1 | 0.3 | 1.2 | 70.8 | 142.5 | 6.7 | 1.4 | 3.5 | 0.2 | 0.4 | 0.0 | 0.3 | 0.0 | 5.5 |
|  | 9 | 10 | 215 | 20.7\% | 33.0 | 10.4 | 0.2 | 0.8 | 52.7 | 103.9 | 5.0 | 1.6 | 2.5 | 0.1 | 0.3 | 0.0 | 0.2 | 0.0 | 3.8 |
|  | 10 | 11 | 136 | 20.6\% | 20.6 | 6.5 | 0.2 | 0.6 | 33.1 | 65.5 | 3.1 | 1.4 | 1.7 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 2.4 |
| NEORB011 | 0 | 1 | 634 | 20.9\% | 99.1 | 30.7 | 0.5 | 1.8 | 158.3 | 312.0 | 13.8 | 2.0 | 6.6 | 0.3 | 0.7 | 0.1 | 0.4 | 0.1 | 7.2 |
|  | 1 | 2 | 592 | 21.4\% | 94.9 | 29.7 | 0.5 | 1.5 | 145.4 | 293.6 | 12.5 | 1.7 | 5.5 | 0.2 | 0.4 | 0.1 | 0.3 | 0.0 | 5.4 |
|  | 2 | 3 | 784 | 21.2\% | 124.8 | 39.1 | 0.6 | 1.9 | 192.3 | 388.2 | 17.5 | 2.3 | 7.7 | 0.3 | 0.6 | 0.1 | 0.4 | 0.1 | 7.7 |
|  | 3 | 4 | 507 | 21.3\% | 81.3 | 25.3 | 0.4 | 1.2 | 123.1 | 251.8 | 10.9 | 1.7 | 4.9 | 0.2 | 0.4 | 0.0 | 0.2 | 0.0 | 5.7 |
|  | 4 | 5 | 181 | 21.4\% | 28.8 | 9.0 | 0.2 | 0.8 | 42.6 | 87.8 | 4.2 | 0.8 | 2.3 | 0.1 | 0.3 | 0.0 | 0.3 | 0.0 | 3.8 |
|  | 5 | 6 | 529 | 21.5\% | 85.3 | 26.0 | 0.5 | 1.7 | 126.7 | 261.6 | 12.5 | 1.7 | 5.7 | 0.2 | 0.4 | 0.0 | 0.3 | 0.0 | 5.9 |
|  | 6 | 7 | 791 | 21.2\% | 126.0 | 39.1 | 0.7 | 2.2 | 194.7 | 390.6 | 18.7 | 1.6 | 8.6 | 0.3 | 0.6 | 0.1 | 0.4 | 0.1 | 8.0 |
|  | 7 | 8 | 88 | 21.4\% | 13.4 | 3.9 | 0.2 | 1.4 | 17.1 | 36.4 | 2.5 | 0.5 | 1.9 | 0.3 | 0.9 | 0.1 | 0.9 | 0.2 | 8.5 |
|  | 8 | 9 | 141 | 22.6\% | 22.5 | 6.3 | 0.4 | 2.7 | 26.2 | 58.5 | 4.2 | 0.6 | 3.4 | 0.5 | 1.3 | 0.2 | 1.4 | 0.2 | 13.0 |
|  | 9 | 10 | 105 | 22.8\% | 16.4 | 4.4 | 0.4 | 2.6 | 17.1 | 38.9 | 3.5 | 0.5 | 2.7 | 0.6 | 1.5 | 0.2 | 1.5 | 0.3 | 13.8 |
|  | 10 | 11 | 102 | 22.2\% | 15.9 | 4.4 | 0.4 | 2.0 | 18.1 | 39.7 | 3.0 | 0.5 | 2.4 | 0.4 | 1.2 | 0.2 | 1.2 | 0.2 | 12.5 |
|  | 11 | 12 | 114 | 22.7\% | 18.3 | 4.9 | 0.4 | 2.3 | 19.9 | 44.2 | 3.6 | 0.5 | 2.9 | 0.6 | 1.4 | 0.2 | 1.3 | 0.2 | 13.5 |
|  | 12 | 13 | 116 | 21.6\% | 17.6 | 4.8 | 0.4 | 2.2 | 20.2 | 43.4 | 3.2 | 0.7 | 2.8 | 0.5 | 1.8 | 0.3 | 1.7 | 0.3 | 16.4 |
|  | 13 | 14 | 141 | 20.9\% | 21.2 | 6.5 | 0.3 | 1.4 | 31.8 | 62.9 | 3.4 | 0.6 | 2.4 | 0.3 | 0.7 | 0.1 | 0.7 | 0.1 | 8.1 |
|  | 14 | 15 | 156 | 21.3\% | 24.4 | 7.4 | 0.2 | 1.1 | 36.0 | 72.7 | 3.9 | 0.6 | 2.3 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 5.9 |
|  | 15 | 16 | 179 | 21.9\% | 28.9 | 8.6 | 0.3 | 1.4 | 40.3 | 82.5 | 4.8 | 0.7 | 3.0 | 0.3 | 0.6 | 0.1 | 0.5 | 0.1 | 7.2 |
|  | 16 | 17 | 159 | 21.9\% | 25.3 | 7.6 | 0.4 | 1.5 | 34.8 | 72.7 | 4.4 | 1.2 | 3.0 | 0.3 | 0.5 | 0.1 | 0.4 | 0.1 | 6.6 |
| NEORB012 | 0 | 1 | 340 | 22.5\% | 54.4 | 16.1 | 1.0 | 5.0 | 77.2 | 137.6 | 9.8 | 2.1 | 7.2 | 0.9 | 2.3 | 0.3 | 1.8 | 0.3 | 24.3 |
|  | 1 | 2 | 273 | 21.6\% | 42.2 | 12.7 | 0.7 | 3.4 | 56.3 | 124.1 | 7.0 | 1.7 | 5.1 | 0.5 | 1.5 | 0.2 | 1.2 | 0.2 | 16.1 |
|  | 2 | 3 | 265 | 19.2\% | 36.7 | 11.3 | 0.4 | 2.3 | 53.4 | 137.6 | 5.9 | 1.6 | 3.6 | 0.4 | 0.9 | 0.1 | 0.7 | 0.1 | 10.1 |
|  | 3 | 4 | 256 | 21.3\% | 39.7 | 12.3 | 0.4 | 2.1 | 58.5 | 119.4 | 6.5 | 1.8 | 3.8 | 0.3 | 0.9 | 0.1 | 0.8 | 0.1 | 9.3 |


| Hole ID | From <br> (m) | To <br> (m) | TREO (ppm) | $\begin{gathered} \text { MREO: } \\ \text { TREO } \\ (\%) \\ \hline \hline \end{gathered}$ | $\begin{aligned} & \hline \mathrm{Nd}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Pr}_{6} \mathrm{O}_{11} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{Tb}_{4} \mathrm{O}_{7}$ (ppm) | $\begin{aligned} & \hline \mathrm{Dy}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{L}_{\mathrm{L}, \mathrm{O}_{8}} \\ & (\mathrm{ppp} \end{aligned}$ | $\begin{gathered} \mathrm{CeO}_{2} \\ (\mathrm{ppm}) \end{gathered}$ | $\begin{aligned} & \mathrm{Sm}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Eu}_{2} \mathrm{O}_{3} \\ & \text { (ppm) } \end{aligned}$ | $\mathrm{Cd}_{2} \mathrm{O}_{3}$ (ppm) | $\mathrm{Ho}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{Er}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{Tm}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{Yb}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{L}_{\mathrm{L}_{2} \mathrm{O}_{3}} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{gathered} \mathrm{Y}_{2} \mathrm{O}_{3} \\ (\text { (ppm) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | 5 | 594 | 21.5\% | 92.6 | 29.2 | 1.0 | 5.1 | 139.6 | 270.2 | 14.5 | 2.5 | 8.1 | 0.9 | 2.3 | 0.3 | 2.2 | 0.3 | 25.0 |
|  | 5 | 6 | 849 | 22.5\% | 138.8 | 43.3 | 1.6 | 7.0 | 193.5 | 386.9 | 22.0 | 3.3 | 12.6 | 1.2 | 3.1 | 0.4 | 2.7 | 0.4 | 32.1 |
|  | 6 | 7 | 666 | 22.9\% | 112.3 | 33.0 | 1.4 | 6.1 | 144.3 | 305.9 | 18.3 | 2.9 | 11.0 | 0.9 | 2.3 | 0.3 | 1.7 | 0.2 | 25.4 |
|  | 7 | 8 | 369 | 23.3\% | 62.4 | 19.2 | 0.8 | 3.6 | 82.6 | 163.4 | 10.7 | 2.3 | 6.6 | 0.5 | 1.2 | 0.1 | 0.8 | 0.1 | 14.6 |
|  | 8 | 12 | 267 | 23.0\% | 44.6 | 13.5 | 0.6 | 2.7 | 58.5 | 117.2 | 7.6 | 1.9 | 4.8 | 0.4 | 1.1 | 0.2 | 0.9 | 0.1 | 13.0 |
|  | 12 | 16 | 498 | 22.6\% | 82.0 | 24.9 | 1.0 | 4.8 | 106.7 | 227.3 | 14.0 | 3.2 | 8.4 | 0.8 | 1.9 | 0.3 | 1.6 | 0.2 | 20.4 |
|  | 16 | 17 | 320 | 22.5\% | 52.7 | 16.2 | 0.6 | 2.6 | 73.5 | 145.0 | 8.9 | 2.2 | 5.0 | 0.4 | 1.1 | 0.1 | 0.8 | 0.1 | 11.0 |
|  | 17 | 18 | 596 | 22.2\% | 98.1 | 29.7 | 0.9 | 3.6 | 137.2 | 278.8 | 15.4 | 2.6 | 7.8 | 0.6 | 1.5 | 0.2 | 1.4 | 0.2 | 18.0 |
|  | 18 | 19 | 496 | 21.9\% | 79.5 | 24.2 | 0.8 | 3.8 | 113.5 | 227.3 | 12.3 | 2.6 | 6.8 | 0.7 | 1.9 | 0.3 | 1.8 | 0.2 | 20.1 |
|  | 19 | 20 | 235 | 24.3\% | 41.2 | 11.9 | 0.7 | 3.3 | 50.7 | 94.6 | 7.5 | 2.3 | 5.4 | 0.5 | 1.3 | 0.2 | 1.2 | 0.2 | 14.5 |
|  | 20 | 21 | 620 | 24.6\% | 110.8 | 32.4 | 1.7 | 7.8 | 132.5 | 258.0 | 19.8 | 4.2 | 12.9 | 1.2 | 3.0 | 0.4 | 2.6 | 0.4 | 32.3 |
|  | 21 | 22 | 356 | 22.6\% | 58.2 | 17.3 | 1.0 | 4.2 | 69.5 | 163.4 | 11.0 | 1.8 | 7.4 | 0.7 | 2.0 | 0.3 | 1.5 | 0.2 | 17.9 |
|  | 22 | 23 | 433 | 21.3\% | 66.7 | 19.3 | 1.1 | 4.8 | 76.5 | 218.7 | 12.3 | 2.2 | 8.3 | 0.7 | 1.7 | 0.3 | 1.6 | 0.2 | 18.0 |
|  | 23 | 24 | 362 | 24.0\% | 62.9 | 18.6 | 1.0 | 4.5 | 72.5 | 159.7 | 11.6 | 2.2 | 7.6 | 0.7 | 1.6 | 0.2 | 1.4 | 0.2 | 17.3 |
|  | 24 | 25 | 755 | 22.5\% | 123.6 | 36.7 | 1.8 | 7.7 | 164.2 | 337.8 | 20.9 | 4.2 | 13.3 | 1.3 | 3.1 | 0.4 | 2.6 | 0.4 | 36.7 |
|  | 25 | 26 | 613 | 24.3\% | 106.6 | 31.4 | 1.8 | 8.8 | 120.8 | 255.5 | 19.4 | 4.7 | 13.3 | 1.5 | 3.9 | 0.5 | 3.5 | 0.5 | 40.5 |
|  | 26 | 27 | 755 | 24.7\% | 134.1 | 39.1 | 2.4 | 11.2 | 150.1 | 309.6 | 25.5 | 7.0 | 17.8 | 1.8 | 4.5 | 0.6 | 3.7 | 0.5 | 47.4 |
|  | 27 | 28 | 290 | 23.2\% | 48.1 | 13.7 | 0.9 | 4.6 | 59.2 | 116.6 | 9.0 | 2.2 | 6.5 | 0.8 | 2.7 | 0.3 | 2.0 | 0.3 | 23.1 |
|  | 28 | 32 | 182 | 23.5\% | 30.6 | 8.4 | 0.6 | 3.2 | 33.8 | 73.9 | 5.6 | 1.6 | 4.3 | 0.7 | 1.6 | 0.2 | 1.3 | 0.2 | 16.0 |
| NEORB013 | 0 | 4 | 277 | 22.0\% | 44.8 | 14.0 | 0.4 | 1.7 | 63.7 | 130.2 | 6.9 | 1.1 | 3.7 | 0.3 | 0.9 | 0.1 | 0.7 | 0.1 | 8.4 |
|  | 4 | 8 | 378 | 21.5\% | 60.7 | 19.1 | 0.4 | 1.2 | 91.7 | 185.5 | 9.1 | 1.0 | 3.8 | 0.2 | 0.3 | 0.0 | 0.2 | 0.0 | 5.0 |
|  | 8 | 12 | 502 | 21.8\% | 81.1 | 26.1 | 0.5 | 1.7 | 116.8 | 249.4 | 11.7 | 1.1 | 5.2 | 0.3 | 0.6 | 0.1 | 0.5 | 0.1 | 7.5 |
|  | 12 | 16 | 457 | 21.6\% | 73.5 | 23.4 | 0.4 | 1.3 | 109.1 | 226.0 | 10.7 | 1.1 | 4.5 | 0.2 | 0.4 | 0.1 | 0.3 | 0.0 | 5.9 |
|  | 16 | 20 | 463 | 21.6\% | 73.8 | 23.7 | 0.5 | 1.9 | 105.3 | 230.9 | 10.4 | 1.1 | 4.9 | 0.3 | 0.7 | 0.1 | 0.5 | 0.1 | 8.8 |
|  | 20 | 24 | 700 | 22.1\% | 114.5 | 36.5 | 0.8 | 2.9 | 158.3 | 346.4 | 16.4 | 1.4 | 7.5 | 0.4 | 1.1 | 0.1 | 0.8 | 0.1 | 12.5 |
|  | 24 | 28 | 778 | 21.9\% | 126.0 | 40.7 | 0.8 | 3.0 | 178.3 | 386.9 | 16.9 | 1.6 | 7.7 | 0.5 | 1.1 | 0.1 | 0.8 | 0.1 | 13.0 |
|  | 28 | 32 | 639 | 21.9\% | 102.5 | 33.6 | 0.7 | 2.9 | 144.3 | 315.7 | 14.4 | 1.4 | 6.7 | 0.5 | 1.2 | 0.1 | 0.9 | 0.1 | 13.7 |
|  | 32 | 36 | 348 | 22.0\% | 56.3 | 17.6 | 0.5 | 2.0 | 77.5 | 167.1 | 9.0 | 1.2 | 4.6 | 0.3 | 0.8 | 0.1 | 0.7 | 0.1 | 9.9 |
|  | 36 | 40 | 500 | 20.4\% | 74.3 | 24.4 | 0.6 | 2.6 | 120.8 | 246.9 | 10.7 | 1.2 | 5.5 | 0.4 | 0.9 | 0.1 | 0.7 | 0.1 | 10.4 |
|  | 40 | 44 | 874 | 22.0\% | 143.5 | 44.3 | 1.0 | 3.9 | 204.1 | 426.3 | 19.0 | 2.1 | 9.1 | 0.6 | 1.5 | 0.2 | 1.2 | 0.2 | 17.3 |
|  | 44 | 48 | 579 | 21.6\% | 93.4 | 28.8 | 0.6 | 2.3 | 132.5 | 287.4 | 14.1 | 1.6 | 6.5 | 0.3 | 0.8 | 0.1 | 0.8 | 0.1 | 9.2 |
|  | 48 | 52 | 1,143 | 21.0\% | 177.3 | 57.6 | 1.2 | 4.4 | 278.0 | 560.2 | 24.1 | 3.5 | 11.4 | 0.7 | 1.8 | 0.2 | 1.3 | 0.2 | 21.2 |
|  | 52 | 56 | 524 | 21.1\% | 82.3 | 26.0 | 0.6 | 1.9 | 129.0 | 253.1 | 12.3 | 1.9 | 5.7 | 0.3 | 0.7 | 0.1 | 0.6 | 0.1 | 9.2 |
|  | 56 | 60 | 594 | 21.2\% | 93.9 | 29.5 | 0.6 | 1.9 | 148.9 | 287.4 | 13.5 | 1.9 | 6.1 | 0.3 | 0.7 | 0.1 | 0.5 | 0.1 | 8.9 |
|  | 60 | 61 | 845 | 21.3\% | 133.0 | 41.2 | 1.2 | 5.0 | 202.9 | 398.0 | 20.2 | 3.6 | 9.4 | 0.8 | 2.1 | 0.3 | 1.9 | 0.3 | 25.4 |
|  | 61 | 62 | 604 | 19.1\% | 80.5 | 24.9 | 1.6 | 8.5 | 137.2 | 249.4 | 14.4 | 2.3 | 10.5 | 1.7 | 4.5 | 0.6 | 3.7 | 0.6 | 63.5 |
|  | 62 | 63 | 200 | 21.9\% | 31.5 | 9.2 | 0.6 | 2.5 | 39.9 | 84.9 | 7.7 | 1.0 | 4.4 | 0.5 | 1.2 | 0.2 | 1.0 | 0.2 | 15.5 |
| NEORB014 | 0 | 4 | 351 | 21.3\% | 55.1 | 17.4 | 0.4 | 2.0 | 86.0 | 167.1 | 8.3 | 1.0 | 3.8 | 0.3 | 0.8 | 0.1 | 0.6 | 0.1 | 8.4 |
|  | 4 | 5 | 208 | 20.6\% | 31.8 | 10.1 | 0.2 | 0.6 | 52.0 | 102.7 | 4.5 | 0.7 | 1.7 | 0.1 | 0.2 | 0.0 | 0.1 | 0.0 | 2.6 |
|  | 5 | 6 | 537 | 21.2\% | 84.4 | 26.9 | 0.5 | 1.7 | 131.4 | 265.3 | 13.0 | 1.0 | 5.0 | 0.2 | 0.5 | 0.1 | 0.3 | 0.0 | 6.9 |
|  | 6 | 7 | 526 | 21.3\% | 83.0 | 26.8 | 0.5 | 1.6 | 126.7 | 262.9 | 12.1 | 1.0 | 4.4 | 0.2 | 0.4 | 0.0 | 0.9 | 0.0 | 5.3 |
|  | 7 | 8 | 839 | 21.5\% | 134.1 | 43.1 | 0.8 | 2.5 | 202.9 | 416.4 | 19.6 | 1.2 | 7.6 | 0.3 | 0.7 | 0.1 | 0.4 | 0.0 | 9.3 |
|  | 8 | 9 | 559 | 21.4\% | 89.1 | 27.7 | 0.6 | 2.1 | 132.5 | 277.6 | 13.8 | 1.0 | 5.6 | 0.3 | 0.6 | 0.1 | 0.4 | 0.0 | 7.4 |
|  | 9 | 10 | 669 | 21.5\% | 106.8 | 34.0 | 0.7 | 2.3 | 160.7 | 331.7 | 15.4 | 1.2 | 6.2 | 0.3 | 0.6 | 0.1 | 0.4 | 0.1 | 9.0 |
|  | 10 | 11 | 1,067 | 22.2\% | 178.5 | 54.4 | 1.0 | 3.2 | 255.7 | 524.5 | 25.4 | 2.1 | 9.9 | 0.4 | 0.8 | 0.1 | 0.6 | 0.1 | 10.9 |
|  | 11 | 12 | 1,502 | 21.8\% | 244.9 | 76.1 | 1.5 | 4.6 | 363.6 | 738.3 | 36.9 | 1.7 | 14.3 | 0.6 | 1.2 | 0.1 | 0.9 | 0.1 | 16.9 |
|  | 12 | 16 | 490 | 21.2\% | 76.6 | 24.4 | 0.6 | 2.3 | 112.6 | 244.5 | 11.8 | 1.3 | 5.0 | 0.3 | 0.8 | 0.1 | 0.6 | 0.1 | 9.4 |
|  | 16 | 17 | 764 | 20.5\% | 115.4 | 36.4 | 1.0 | 3.8 | 183.0 | 373.4 | 17.9 | 3.1 | 8.3 | 0.6 | 1.5 | 0.2 | 1.1 | 0.2 | 18.3 |
|  | 17 | 18 | 2,189 | 21.3\% | 345.3 | 111.6 | 2.0 | 7.0 | 538.3 | 1,071.2 | 50.4 | 4.7 | 19.9 | 1.0 | 2.4 | 0.3 | 1.8 | 0.3 | 32.6 |
|  | 18 | 19 | 1,210 | 21.4\% | 192.5 | 60.9 | 1.3 | 4.6 | 289.7 | 593.3 | 29.1 | 2.7 | 11.5 | 0.7 | 1.6 | 0.2 | 1.4 | 0.2 | 20.7 |
|  | 19 | 20 | 1,503 | 23.3\% | 261.3 | 80.6 | 1.9 | 6.6 | 336.6 | 722.3 | 42.7 | 4.1 | 16.1 | 0.9 | 2.2 | 0.3 | 1.7 | 0.2 | 25.4 |
|  | 20 | 21 | 1,062 | 25.1\% | 198.3 | 55.1 | 2.5 | 10.8 | 204.1 | 460.7 | 40.1 | 4.9 | 20.1 | 1.7 | 4.5 | 0.6 | 3.6 | 0.5 | 55.1 |
|  | 21 | 22 | 2,827 | 27.5\% | 587.9 | 163.1 | 5.4 | 20.5 | 472.6 | 1,314.4 | 107.7 | 8.2 | 45.0 | 3.1 | 7.5 | 1.0 | 6.1 | 0.9 | 83.6 |
|  | 22 | 23 | 454 | 21.4\% | 72.0 | 22.5 | 0.6 | 2.4 | 103.3 | 219.9 | 11.4 | 1.7 | 5.1 | 0.4 | 1.0 | 0.1 | 0.8 | 0.1 | 13.1 |
|  | 23 | 24 | 1,157 | 22.2\% | 190.1 | 59.9 | 1.4 | 5.1 | 262.7 | 565.1 | 28.6 | 4.1 | 11.3 | 0.8 | 2.0 | 0.3 | 1.6 | 0.2 | 23.2 |
|  | 24 | 25 | 932 | 21.0\% | 144.6 | 46.5 | 1.0 | 3.7 | 228.7 | 458.2 | 19.7 | 2.7 | 8.0 | 0.5 | 1.4 | 0.2 | 1.0 | 0.1 | 15.4 |

## VOLTAIC

| Hole ID | $\begin{aligned} & \hline \text { From } \\ & (\mathrm{m}) \end{aligned}$ | $\begin{aligned} & \hline \text { To } \\ & (\mathrm{m}) \end{aligned}$ | TREO (ppm) | $\begin{gathered} \text { MREO: } \\ \text { TREO } \\ (\%) \\ \hline \hline \end{gathered}$ | $\mathrm{Nd}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \hline \mathrm{Pr}_{6} \mathrm{O}_{11} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{Tb}_{4} \mathrm{O}_{7}$ (ppm) | $\begin{aligned} & \begin{array}{l} \mathrm{Dy}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{array} \end{aligned}$ | $\begin{aligned} & \mathrm{La}_{\mathrm{o}} \mathrm{O}_{\mathrm{s}} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{CeO}_{2} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Sm}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{E}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Cd}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{HO}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{Er}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\mathrm{Tm}_{2} \mathrm{O}_{3}$ (ppm) | $\begin{aligned} & \mathrm{Yb}_{2} \mathrm{O}_{3} \\ & (\mathrm{ppm}) \end{aligned}$ | $\begin{aligned} & \mathrm{Lu}_{2} \mathrm{O}_{8} \\ & (\mathrm{ppmm}) \end{aligned}$ | $\begin{gathered} \mathrm{Y}_{2} \mathrm{O}_{3} \\ (\mathrm{ppm}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 25 | 26 | 1,245 | 20.5\% | 189.0 | 60.8 | 1.1 | 4.0 | 320.2 | 609.3 | 26.7 | 2.9 | 10.8 | 0.6 | 1.4 | 0.2 | 1.0 | 0.1 | 17.0 |
|  | 26 | 27 | 797 | 21.4\% | 128.3 | 39.7 | 0.6 | 1.7 | 197.0 | 396.8 | 18.0 | 2.2 | 6.2 | 0.2 | 0.4 | 0.0 | 0.4 | 0.0 | 5.2 |
|  | 27 | 28 | 1,116 | 21.5\% | 178.5 | 54.5 | 1.3 | 5.3 | 273.3 | 525.8 | 27.3 | 5.7 | 12.0 | 0.8 | 2.1 | 0.3 | 1.8 | 0.3 | 27.7 |
|  | 28 | 29 | 1,439 | 21.4\% | 229.8 | 73.7 | 1.1 | 3.1 | 360.0 | 710.0 | 32.7 | 3.0 | 11.6 | 0.4 | 0.9 | 0.1 | 0.7 | 0.1 | 11.7 |
|  | 29 | 30 | 929 | 21.8\% | 151.6 | 47.7 | 0.8 | 2.2 | 221.7 | 464.3 | 22.4 | 2.0 | 7.8 | 0.3 | 0.6 | 0.1 | 0.4 | 0.1 | 7.0 |
|  | 30 | 31 | 1,944 | 21.6\% | 316.1 | 98.6 | 1.5 | 4.0 | 477.3 | 968.0 | 45.0 | 2.8 | 15.9 | 0.5 | 0.9 | 0.1 | 0.7 | 0.1 | 12.2 |
|  | 31 | 32 | 635 | 21.1\% | 99.4 | 31.7 | 0.6 | 2.1 | 148.9 | 320.6 | 14.8 | 1.5 | 5.7 | 0.3 | 0.6 | 0.1 | 0.4 | 0.1 | 7.8 |
|  | 32 | 36 | 913 | 21.7\% | 147.0 | 46.8 | 1.0 | 3.6 | 215.8 | 448.4 | 20.8 | 2.2 | 8.3 | 0.5 | 1.3 | 0.2 | 1.1 | 0.1 | 15.6 |
|  | 36 | 37 | 825 | 21.8\% | 133.0 | 42.2 | 0.9 | 3.8 | 191.2 | 407.8 | 17.7 | 2.0 | 7.5 | 0.6 | 1.4 | 0.2 | 1.1 | 0.2 | 15.4 |
|  | 37 | 38 | 942 | 21.5\% | 150.5 | 46.6 | 1.1 | 4.3 | 220.5 | 465.6 | 21.2 | 2.3 | 8.9 | 0.7 | 1.6 | 0.2 | 1.3 | 0.2 | 17.3 |
|  | 38 | 39 | 924 | 21.9\% | 150.5 | 46.6 | 1.1 | 4.4 | 218.1 | 448.4 | 19.6 | 2.4 | 8.6 | 0.7 | 1.8 | 0.2 | 1.3 | 0.2 | 20.3 |
|  | 39 | 40 | 765 | 21.5\% | 121.3 | 37.2 | 1.0 | 4.6 | 171.2 | 374.7 | 18.0 | 1.9 | 9.1 | 0.7 | 2.0 | 0.2 | 1.4 | 0.2 | 21.5 |
|  | 40 | 41 | 818 | 21.1\% | 127.1 | 39.6 | 1.1 | 4.7 | 184.1 | 405.4 | 18.9 | 1.9 | 9.8 | 0.7 | 1.9 | 0.3 | 1.5 | 0.2 | 20.6 |
|  | 41 | 42 | 842 | 21.5\% | 134.1 | 42.0 | 0.9 | 3.9 | 188.8 | 421.3 | 19.5 | 1.9 | 9.5 | 0.6 | 1.4 | 0.2 | 1.0 | 0.2 | 16.5 |
|  | 42 | 43 | 434 | 20.6\% | 66.0 | 21.1 | 0.5 | 1.9 | 101.6 | 216.2 | 9.8 | 1.5 | 4.7 | 0.3 | 0.7 | 0.1 | 0.6 | 0.1 | 9.1 |
|  | 43 | 44 | 625 | 21.3\% | 99.1 | 30.4 | 0.7 | 3.0 | 137.2 | 314.5 | 14.8 | 1.8 | 7.1 | 0.4 | 1.0 | 0.1 | 0.9 | 0.1 | 13.2 |
|  | 44 | 48 | 643 | 21.8\% | 104.4 | 32.3 | 0.7 | 3.0 | 137.2 | 325.5 | 14.8 | 2.3 | 7.0 | 0.4 | 1.2 | 0.2 | 1.0 | 0.1 | 12.8 |
|  | 48 | 52 | 786 | 21.8\% | 127.1 | 39.3 | 1.0 | 3.9 | 168.9 | 394.3 | 19.6 | 3.3 | 9.1 | 0.6 | 1.4 | 0.2 | 1.0 | 0.1 | 16.3 |
|  | 52 | 53 | 1,525 | 20.3\% | 223.9 | 73.1 | 2.1 | 10.1 | 360.0 | 739.5 | 32.8 | 4.6 | 17.3 | 1.7 | 4.9 | 0.7 | 4.0 | 0.6 | 49.8 |
|  | 53 | 54 | 551 | 21.6\% | 87.5 | 26.9 | 0.9 | 3.7 | 120.8 | 265.3 | 14.3 | 3.2 | 7.8 | 0.6 | 1.5 | 0.2 | 1.0 | 0.2 | 17.3 |
|  | 54 | 55 | 404 | 21.3\% | 63.8 | 19.9 | 0.4 | 1.8 | 92.4 | 199.0 | 9.2 | 2.1 | 4.3 | 0.3 | 0.9 | 0.1 | 0.6 | 0.1 | 9.0 |
|  | 55 | 56 | 2,122 | 21.3\% | 335.9 | 106.4 | 2.2 | 8.3 | 492.6 | 1,054.0 | 49.9 | 5.5 | 22.7 | 1.3 | 3.2 | 0.4 | 2.7 | 0.4 | 36.6 |
|  | 56 | 57 | 1,082 | 21.5\% | 173.8 | 53.9 | 1.0 | 3.8 | 248.6 | 539.3 | 24.8 | 2.8 | 11.0 | 0.6 | 1.5 | 0.2 | 1.2 | 0.2 | 19.3 |
|  | 57 | 58 | 872 | 21.3\% | 138.8 | 42.6 | 0.9 | 3.5 | 197.0 | 438.5 | 19.7 | 2.9 | 8.9 | 0.5 | 1.3 | 0.2 | 1.2 | 0.2 | 16.1 |
|  | 58 | 59 | 244 | 18.0\% | 31.8 | 10.0 | 0.4 | 1.7 | 66.4 | 113.9 | 5.6 | 1.2 | 3.4 | 0.3 | 0.7 | 0.1 | 0.5 | 0.1 | 8.1 |
|  | 59 | 60 | 140 | 21.2\% | 21.6 | 6.6 | 0.2 | 1.2 | 32.1 | 64.0 | 4.1 | 1.1 | 2.5 | 0.2 | 0.5 | 0.1 | 0.4 | 0.1 | 5.1 |

## Appendix B JORC Tables

Section 1 Sampling Techniques and Data

| Criteria | JORC Code explanation | Commentary |
| :---: | :---: | :---: |
| Sampling techniques | - Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. <br> - Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. <br> - Aspects of the determination of mineralisation that are Material to the Public Report. <br> - In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information. | - Historical and recent $\mathrm{AC} / \mathrm{RB} / \mathrm{RC}$ drill samples were collected at 1 m intervals and composited to 4 m lengths for analysis. The 4 m composite or 1 m sample (where submitted) were crushed and a sub-fraction obtained for pulverisation. <br> - Rock chip samples were taken as individual rocks representing an outcrop (or grab samples). Surface rock samples can be biased towards higher grade mineralisation. <br> - Historical drillcore sampling was completed throughout drillholes by compositing variable widths (predominantly 5 m ) with a representative 5 cm half core sample, representing each respective drill meter. <br> - Drillholes were located using hand-held GPS. <br> - Sampling was carried out under Voltaic Strategic Resources Ltd protocols and QAQC procedures as per current industry practice. <br> - RC drilling was used to obtain 1 m samples collected through a splitter into buckets and placed in bags as 1 m samples, in rows of 20 . <br> - Sample quality was supervised with any sample loss or moisture recorded. <br> - Composite samples were collected with a scoop to generate composite samples. <br> - Samples will be or have been dispatched to LabWest laboratories in Perth. <br> - All samples will be analysed using Microwave digest (MD), Inductively Coupled Plasma Mass Spectrometry and Inductively Coupled Plasma (ICP) Mass Spectrometry (MS) and Optical Emission Spectrometry (OES) to finish. 62 element analysis including REEs by ICP-MS/OES. |
| Drilling techniques | - Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc). | - AC/RC drilling was completed by PNC Exploration/ESSO/Cameco utilising AC/RC drill methods. <br> - Historical drilling by Cameco used Wallis Drilling to undertake diamond drilling using a UDR-1000 drill rig. The drilling was completed using $\mathrm{HQ}(63.5 \mathrm{~mm}) \& \mathrm{NQ}(47.6 \mathrm{~mm})$ from surface for the collection of drill core samples. <br> - Current $R B$ drilling was carried out utilising a slimline $A C$ rig combining $R C$ drill rod string with a blade from surface to basement. <br> - Prior Auger Vacuum (AV) drilling was carried out with an auger mounted tractor |
| Drill sample recovery | - Method of recording and assessing core and chip sample recoveries and results assessed. <br> - Measures taken to maximise sample recovery and ensure representative nature of the samples. Whether a relationship exists between sample recovery \& grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material. | - Cameco reported drill recoveries as being close to $100 \%$ for the historical drilling. <br> - Historical drill core sample bias has occurred given only 5 cm of respective 1 m core sample interval run was submitted through composite sampling. <br> - A review is being undertaken to assess the potential to re-submit entire mineralised intervals where drill core has been found \& identified, \& interval runs remain complete. |
| Logging | - Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. <br> - Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. <br> - The total length and percentage of the relevant intersections logged. | - Current drilling is being logged to industry standard capturing recoveries, regolith logging, mineralisation, pXRF and CPS (radiation) monitoring Cameco logged drill holes for geology, mineralisation, structure, and alteration. The geological and geotechnical logging is consistent with industry standards. |
| Sub-sampling techniques and sample preparation | - If core, whether cut or sawn and whether quarter, half or all core taken. <br> - If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. <br> - For all sample types, the nature, quality and appropriateness of the sample | - Current sampling includes comprehensive and industry standard QAQC inclusive of split and duplicate samples, and applicable and representative REE standards. <br> - Historical drillcore sampling was completed throughout drillholes by compositing variable widths (predominantly 5 m ) with a representative a 5 cm half core sample, representing each respective drill |

Criteria
JORC Code explanation
preparation technique

- Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.
- Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.
- Whether sample sizes are appropriate to the grain size of the material being sampled.

Quality of assay data and laboratory tests

- The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.
- For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.
- Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.

Commentary

- Sampling measured spectral parameters using the PIMA II spectrometer and also assayed as lithologybased composites.
- pXRF analysis of $\mathrm{AV} / \mathrm{RB} / \mathrm{RC}$ sample piles is deemed fit for purpose as a preliminary exploration technique. pXRF provides a spot reading on sample piles with variable grain sizes and states of homogenisation. Hig grade results were repeated at multiple locations to confirm repeatability. The competent person considers this acceptable within the context of reporting preliminary exploration results.
- Recent drill samples were analysed by Labwest Minerals Analysis Pty Ltd in Perth. The sample analysis uses multi-acid microwave digest with an Inductively Coupled Plasma Mass Spectrometry and Inductively Coupled Plasma (ICP) Mass Spectrometry (MS) and Optical Emission Spectrometry (OES) finish.
- Historical Cameco drill core samples were analysed by Chemnorth using four assay methods, ICP-OES, CP-MS, AAS and gravity to analyse $32-53$ elements.
- pXRF screening of samples and soil points preliminary analysis is obtained with an Olympus Vanta portable XRF
- NOTE 1: pXRF (portable x-ray fluorescence) assay results are semi-quantitative only.

NOTE 2: pXRF - Only 5 elements analysed with pXRF analyser: Ce, La, Nd, Pr, Y

- Scanning electron microscope (SEM) analysis was undertaken by RSC Consulting Limited at their West Perth office using a Hitachi SU-3900 instrument which is capable of delivering automated mineralogy using the Advanced Mineral Identification and Characterisation System (AMICS). The instrument has detectors for analysing energy dispersive spectrometry (EDS), backscatter electron (BSE), secondary electron (SE) and can run on ultra-variable pressure (UVD).
- RSC undertook an initial characterisation study of eleven (11) smear clay, three (3) epoxy resin embedded clay and two (2) basement rock samples of historical drillcore (GADO004 hole) from the company's Paddys Well REE project to investigate the mineralogical distribution of REE within the mineralised clay and vein horizons. RSC used their optical microscope and SEM for this work. Microcharacterisation of and vein horizons. RSC used their optical microscope and SEM for this work. Microcharacterisation of
the samples provide an understanding of REE distribution and the potential implications for eventual metallurgical performance.

| Criteria | JORC Code explanation | Commentary |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Verification of sampling and assaying | - The verification of significant intersections by either independent or alternative company personnel. <br> - The use of twinned holes. <br> - Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. <br> - Discuss any adjustment to assay data. | - Analytical QC is monitored by the laboratory using standards and repeat assays. <br> - Independent standards were submitted by the Company at a rate of 1:25 samples. <br> - Independent field duplicates were not conducted for and were not considered necessary for this early stage of exploration. <br> - The procedures used for verification of historical Cameco sampling and assaying are not known. <br> - Rare earth element analyses were originally reported in elemental form but have been converted to relevant oxide concentrations as per industry standards: $\begin{array}{ll} -\quad & \text { TREO }=\mathrm{La}_{2} \mathrm{O}_{3}+\mathrm{CeO}_{2}+\mathrm{Pr}_{6} \mathrm{O}_{11}+\mathrm{Nd}_{2} \mathrm{O}_{3}+\mathrm{Sm}_{2} \mathrm{O}_{3}+\mathrm{Eu}_{2} \mathrm{O}_{3}+\mathrm{Gd}_{2} \mathrm{O}_{3}+\mathrm{Tb}_{4} \mathrm{O}_{7}+\mathrm{Dy}_{2} \mathrm{O}_{3}+\mathrm{Ho}_{2} \mathrm{O}_{3}+\mathrm{Er}_{2} \mathrm{O}_{3} \\ & +\mathrm{Tm}_{2} \mathrm{O}_{3}+\mathrm{Yb}_{2} \mathrm{O}_{3}+\mathrm{Lu}_{2} \mathrm{O}_{3}+\mathrm{Y}_{2} \mathrm{O}_{3} \\ -\quad & \text { MREO }=\mathrm{Pr}_{6} \mathrm{O}_{11}+\mathrm{Nd}_{2} \mathrm{O}_{3}+\mathrm{Dy}_{2} \mathrm{O}_{3}+\mathrm{Tb}_{4} \mathrm{O}_{7} \end{array}$ <br> Conversion factors used to convert from element to oxide: |  |  |
|  |  | Element | Oxide Conversion Factor | Equivalent Oxide |
|  |  | Ce | 1.2284 | $\mathrm{CeO}_{2}$ |
|  |  | Dy | 1.1477 | $\mathrm{Dy}_{2} \mathrm{O}_{3}$ |
|  |  | Er | 1.1435 | $\mathrm{Er}_{2} \mathrm{O}_{3}$ |
|  |  | Eu | 1.1579 | $\mathrm{Eu}_{2} \mathrm{O}_{3}$ |
|  |  | Gd | 1.1526 | $\mathrm{Gd}_{2} \mathrm{O}_{3}$ |
|  |  | Ho | 1.1455 | $\mathrm{Ho}_{2} \mathrm{O}_{3}$ |
|  |  | La | 1.1728 | $\mathrm{La}_{2} \mathrm{O}_{3}$ |
|  |  | Lu | 1.1371 | $\mathrm{Lu}_{2} \mathrm{O}_{3}$ |
|  |  | Nd | 1.1664 | $\mathrm{Nd}_{2} \mathrm{O}_{3}$ |
|  |  | Pr | 1.2082 | $\mathrm{Pr}_{6} \mathrm{O}_{11}$ |
|  |  | Sc | 1.5338 | $\mathrm{Sc}_{2} \mathrm{O}_{3}$ |
|  |  | Sm | 1.1596 | $\mathrm{Sm}_{2} \mathrm{O}_{3}$ |
|  |  | Tb | 1.1762 | $\mathrm{Tb}_{4} \mathrm{O}_{7}$ |
|  |  | Tm | 1.1421 | $\mathrm{Tm}_{2} \mathrm{O}_{3}$ |
|  |  | Y | 1.2699 | $\mathrm{Y}_{2} \mathrm{O}_{3}$ |
|  |  | Yb | 1.1387 | $\mathrm{Yb}_{2} \mathrm{O}_{3}$ |
| Location of data points | - Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. <br> - Specification of the grid system used. <br> - Quality and adequacy of topographic control. | - The Cameco holes were surveyed using the UTM coordinate system. The survey method and accuracy were not reported. <br> - Downhole surveys were completed using an Eastman downhole survey tool. <br> - Recent drilling is captured via GPS on GDA Z50 coordinates |  |  |
| Data spacing and distribution | - Data spacing for reporting of Exploration Results. <br> - Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. <br> - Whether sample compositing has been applied. | - Cameco early-stage exploration was completed to verify previous explorers interpretation and pursue lateral extents of uranium mineralisation. <br> - Neo drill spacing was undertaken on an initial $80 \times 40 \mathrm{~m}$ <br> - Regional soil pXRF survey was undertaken on a wide space $200 \times 80 \mathrm{~m}$ |  |  |
| Orientation of data in relation to geological structure | - Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. <br> - If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material. | - The drilling that has been completed to date has not been structurally reviewed or validated to confirm the orientation of interpreted mineralisation <br> - Rock chip samples were selected to target specific geology, alteration and mineralisation. The samples were collected to assist historical explorers develop their understanding of the geology and exploration potential of historical tenure. <br> - Drill orientations have targeted interpreted mineralised horizons and lithological boundaries, as |  |  |


| Criteria | JORC Code explanation | Commentary |
| :---: | :---: | :---: |
|  |  | perpendicular as possible. <br> - Oxide regolith drilling is vertical |
| Sample security | - The measures taken to ensure sample security. | - Sample security was not reported by Cameco. Samples were given individual samples numbers for tracking. <br> - Recent drilling and surface sample security and integrity is in place to industry standards |
| Audits or reviews | - The results of any audits or reviews of sampling techniques and data. | - The sampling techniques and analytical data are monitored by the Company's geologists. <br> - A review of the historical core and compiled data is being undertaken to confirm historical results and assist in interpretation and targeting of further exploration. |

## Section 2 Reporting of Exploration Results

## (Criteria listed in the preceding section also apply to this section.)

## Criteria

Mineral tenement
and land tenure and land tenure status

- Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.
- The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.
- Acknowledgment and appraisal of exploration by other parties.

Commentary
The project area is located approximately 60 km northeast of the Gascoyne Junction and 220km east of Carnarvon.

- The Paddys Well project comprises one granted Exploration Licence, E09/2414 (where all of the current reported activities too place) and four Exploration Licence Applications E 09/2663, E 09/2669, E 09/2774, E 09/2744, E 09/2773.
- The tenements lie within Native Title Determined Areas of the Yinggarda, Baiyungu and Thalanyji People and Gnulli People.
- All the tenements are in good standing with no known impediments.
- Numerous exploration campaigns have been completed in the general area since the early 1970's focusing predominantly on uranium and diamonds, however work within tenement area E09/2414 has been limited and there is no documented exploration targeting rare earth elements or lithium.
- From 1974-1983 companies including Uranerz, Agip Nucleare, AFMECO, ESSO Minerals and Urangesellschaft explored the Gascoyne Region for uranium with little success. Most anomalies identified were limited to secondary uranium occurrences in basement metamorphic sequences (including some occurrences
- Subsequently from 1992 - 1996, PNC Exploration explored the southern Gascoyne area actively targeting basement-hosted uranium mineralisation within the Morrissey Metamorphics (WAMEX REPORT A 46584).
- The exploration focussed on determining the source of $U$ anomalies and their association with EM conductors traverses across regional gealy in line Additional EM was flown as well as detailed airborne radionetrics, traverses across regional geological trends. Additional EM was fown, as well as detailed airborne radiometrics, which identified several anomalies (WAMEX REPORT A 49947). Eleven (11) shallow percussion holes (average
 calc-silc $10514: 22-28 \mathrm{~m}(6 \mathrm{~m})$ a 653 pm .

GA9515: $16-25 \mathrm{~m}(9 \mathrm{~m})$ at $335 \mathrm{ppm} U$ U .

- GA9520: 19-28m ( 9 m ) at 633 ppm U , including 0.5 m at $3900 \mathrm{ppm} \mathrm{U}(25.25 \mathrm{~m}-25.75 \mathrm{~m})$ and 0.25 m at $1000 \mathrm{ppm} \mathrm{U}(26.50-26.75 \mathrm{~m})$.
- Test work determined that both secondary and primary (uraninite) mineralisation is present, and that the chemical signature of the chlorite alteration is similar to that at Jabiluka. A follow-up program of RC drilling in 1996 (17 holes $/ 1217 \mathrm{~m}$ ) returned several well mineralised intercepts at the main anomaly:
- GAR9630: 41-49m (8m) at 860 ppm U , including 1 m at 3700 ppm U , and $53-58 \mathrm{~m}(5 \mathrm{~m})$ at 568 ppm U GAR9630: 41-49m (8m) at 860 ppm
from 53m, incl. 1 m at 1200 ppm U ).
GAR9625: 22-26m (4m) at 585 ppm U , including 1 m at 1800 ppm U
- GAR9626: 20-29m ( 9 m ) at 275 ppm U.
- In 1999 Cameco completed a programme of two diamond holes for a total of 411 m , followed by another four diamond drill holes for a total of 863.3 m in 2000 . The drilling programme aimed to test depth and lateral extensions to the mineralisation identified in the percussion holes; however, it failed to return intercepts of economic uranium grades. Cameco concluded that the strong structural disruption, radiometric response (peaked at 58 ppm U ) and presence of graphite appear to be favourable for uranium mineralisation but went on to say that the minor remobilisation of radiogenic lead sourced from the decay of uranium downgrades the potential of the area. Core samples were systematically analysed with a Portable Infrared Mineral Analyse (PIMA) and sent for petrophysical and petrographic characterisation as well as for Pb isotopes studies (WAMEX REPORT A 61566). Despite the presence of some marked hydrothermal alteration along brittle small scale structures, it failed to identify potential indicators of significant uranium mineralisation.
- U308 Limited reviewed the area from 2006-2010, and carried out an airborne magnetic and radiometric surveys, as well as reconnaissance field work with grab sampling for geochemical and petrographic studies. A total of nineteen (19) samples were sent for geochemical analysis to ALS-Chemex in Perth for trace element-

VOLTAIC

| Criteria |
| :--- |
| Geology |
|  |
|  |

JORC Code explanation
Commentary
and whole-rock characterisation. The presence of coincidently elevated $\mathrm{U}, \mathrm{V}, \mathrm{Zn}$, and Sr values in sample 471
is consistent with a strongly weathered black shale (WAMEX REPORT A 84272).

- The project area has historically been considered prospective for unconformity vein style uranium, although it equally considered prospective for rare earth element (REE) mineralisation hosted in iron-rich carbonatite dykes or intrusions, or lithium-caesium-tantalum (LCT) pegmatites.
- The project area encompasses a portion of the Gascoyne Province of the Capricorn Orogen. This geological belt is positioned between the Archaean Yilgarn Craton to the south, and the Archaean Pilbara Craton to the north, and largely consists of a suite of Archaean to Proterozoic gneisses, granitic and metasedimentary rocks.
- REE discoveries in the Gascoyne area, such as Yangibana, are associated with ironstone (weathered ferrocarbonatite) host rocks whereby weathering has enriched the REEs in situ. Yangibana is approximately 100 km NE from the Paddys Well/West Wel project area and contains widespread occurrence of ironstone峟 Ferrocarbonalle Complex, which is located Noand , e Durlacher Supersuite and metasedmentary rocks of hooranoo Metamorphics.
- The ironstone dykes are commonly surrounded by narrow haloes of fenitic alteration, and locally associated with quartz veining. Fenite is a metasomatic alteration associated particularly with carbonatite intrusions
- Drill collar and survey data are provided, along with various respective metadata. Historic drill holes collar and interval data were previously reported by Cameco and are available in open file (WAMEX REPORT A 61566). results including a tabulation of the following information for all Material drill holes. easting and northing of the drill hole collar
- elevation or RL (Reduced Level - elevation above sea level in metres) of the drill hole collar
dip and azimuth of the hole
- down hole length and interception depth
- hole length.
- If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.
- In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.
- Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.
- The assumptions used for any reporting of metal equivalent values should be clearly stated.
- These relationships are particularly important in the reporting of Exploration Results.
- If the geometry of the mineralisation with respect to the drill hole angle is known its nature should be reported.
- If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known')


## VOLTAIC

## Criteria

Diagrams

Balanced reporting

Other substantive exploration data

Further work

## JORC Code explanation

- Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.
- Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.
- Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.
- The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).
- Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.


## Commentary

- Historical map plan figures were registered utilising 2-D software and respective coordinate datums.
- Hole drill collar ground truthing is expected to fine-tune actual collar positions.

Workspaces of current and historical exploration have been constructed utilising 2\&3D GIS software

- No inference to economic mineralisation has been stated
- A cut-off of 250ppm TREO was used in reporting of exploration results, to aid dismissing interpreted unrealistic anomalous mineralised sub-zones.
- All of the relevant historical exploration data has been included in this report
- All historical exploration information is available via WAMEX.
- On-going field reconnaissance exploration in the area continues and is a high priority for the Company.
- Exploration is likely to include further lithological and structural mapping; rockchip sampling; acquisition of high-resolution geophysical radiometric and magnetic data to assist geological interpretation, target identification; as well as auger and percussion drilling of ranked drill targets.


[^0]:    ${ }^{1}$ Based on stated TREO cutoff and a preliminary review of several peer company announcements. Please see Forward Looking cautionary statement on page 5 \& JORC tables.
    ${ }^{2}$ TREO: Total Rare Earth Element Oxide including yttrium oxide ( $\mathrm{Y}_{2} \mathrm{O}_{3}$ ); MREO:TREO: the ratio of "Magnet" REEs to Total REEs in oxide form. "Magnet" REEs = Nd, Pr, Tb, Dy
    ${ }^{3}$ Refer ASX:VSR release dated 13 October 2022 'Rare Earths Confirmed at Gascoyne Project'
    ${ }^{4} \mathrm{An}$ ASX announcement is currently being prepared to provide an update on these results.

[^1]:    ${ }^{5}$ Refer ASX:VSR release dated 17 April 2023 'Met test work on REE-enriched clays at Paddys Well' \& ASX:VSR release dated 17 May 2023 'Drilling confirms significant Rare Earths system at Neo'

[^2]:    ${ }^{6}$ This program comprised 14 RB holes for 710 m at Neo, and 8 holes for 405 m at Link, with assays for Link holes pending

[^3]:    * NOTE: cutoff of 250ppm TREO used

[^4]:    ${ }^{7}$ Both halloysite (needles) and kaolinite (plates) are seen here intergrown with a REE-phosphate grain (bright phase on the right). The association between the minerals suggests that the REE phosphate formed contemporaneously with the clay minerals or after clay formation indicating that the REE phosphate is a secondary REE mineral and not a detrital REE phase.
    ${ }^{8}$ Refer ASX release date 13 October 2022 ‘REEs confirmed at Paddys Well'
    ${ }^{9}$ Qiu S, Yan H, Hong B, Long Q, Xiao J, Li F, Tong L, Zhou X, Qiu T 2022, 'Desorption of REEs from Halloysite and Illite: A Link to the Exploitation of lonAdsorption RE Ore Based on Clay Species', Minerals, vol. 12, no. 8, https://doi.org/10.3390/min12081003.

